ASC-TR-95-1004

# MARK IIA AQUEOUS FILM FORMING FOAM (AFFF) PRECISION METERING SYSTEM PRODUCT EVALUATION TEST REPORT

Aeronautical Systems Center Weapons, Air Base and Range Product Support Office ASC/VXO 314 W. Choctawhatchee Ave., Ste. 104 Eglin AFB FL 32542-5717



August 1995

FINAL REPORT FOR PERIOD 16 DECEMER 1992 - 9 NOVEMBER 1994

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#### ABBREVIATIONS/ACRONYMS/SYMBOLS

AQUEOUS FILM FORMING FOAM AFFF AFR AIR FORCE REGULATION APPLIED RESEARCH ASSOCIATES, INC. ARA ARFF AIRCRAFT RESCUE AND FIREFIGHTING VEHICLE OPERATIONAL AVAILABILITY Αo BDM MANAGEMENT SYSTEMS COMPANY BDM DOD DEPARTMENT OF DEFENSE DSN DEFENSE SWITCHING NETWORK **GALLONS PER MINUTE** gpm IN ACCORDANCE WITH IAW LTI LIMITED TECHNICAL INSPECTION THE COMPUTERIZED FOAM PROPORTIONING SYSTEM (PRODUCED BY MARK IIA NORDIC SYSTEMS INC.) MDT MEAN DOWN TIME MEAN TIME BETWEEN MAINTENANCE MTBM NATIONAL FIRE PROTECTION ASSOCIATION NFPA P-19 A/S32P-19 CRASH FIRE RESCUE VEHICLE PROGRAM MANAGEMENT DIRECTIVE PMD RELIABILITY, MAINTAINABILITY, AND AVAILABILITY RM&A RTO RESPONSIBLE TEST ORGANIZATION

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RESCUE SYSTEMS SECTION

WL/FIVCF

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## SECTION I PURPOSE AND BACKGROUND

- 1.0 **PURPOSE.** The purpose for this product evaluation was to examine an off-the-shelf aqueous film forming foam (AFFF) metering system for incorporation on Air Force Crash Fire Rescue Vehicles. This product evaluation was accomplished as part of a continuing effort to identify an AFFF system capable of metering foam accurately at 1%, 3% and 6% concentrations. The results of this evaluation will support a decision to apply the technology to Air Force firefighting apparatus. If applicable, the Department of Defense (DOD) could use the results of the evaluation for other firefighting vehicles.
- 1.1 <u>AUTHORIZING DIRECTIVES</u>. Authority for the Mark IIA system product evaluation is in PMD 8028(9), dated 10 May 1991. This evaluation was conducted as directed in AFR 80-14 and AFR 55-43.
- 1.2 BACKGROUND. The DOD currently uses AFFF concentrates formulated and mixed with water in ratios of 3 and 6 percent, using an around-the-pump proportioning system with fixed orifices. Common fire protection community terminology refers to an AFFF concentrate designed to be mixed with water at a ratio of 3% AFFF to 97% water as "3% AFFF". A "6% AFFF" concentrate contains approximately one-half of the surfactant and other active ingredients as 3% AFFF concentrate per unit volume and, consequently, is referred to as "less concentrated". When mixed with water at their designed ratios, both types AFFF/water mixture are essentially the same. The newest commercial AFFF formulation is 1% concentrate which is increasingly being used by civilian firefighting facilities. By using 1.0% AFFF concentrate (as compared to 3% and 6%), a considerable cost savings in shipping and storage can be achieved. Likewise, agent conservation, extended firefighting capability, and reduced environmental impact can be realized. Although the Air Force inventory is 3% AFFF, 6% foam concentrate was evaluated to provide system performance data when the Air Force must acquire 6.0% foam such as was done during Operation Desert Shield/Storm. To enhance the interoperability of Air Force firefighting equipment during contingency applications, an additional capability to use 1% AFFF is highly advocated.
- 1.3 <u>DESCRIPTION OF SYSTEM TESTED</u>. The Nordic Systems Inc. Mark IIA Computerized Foam Proportioning System (hereafter called the Mark IIA) is a computer controlled metering system that continually adjusts the foam flow to deliver the correct solution concentration. Nordic Systems Inc. personnel installed and calibrated the Mark IIA system on a WL/FIVCF P-19 firefighting vehicle and provided operator and maintenance training to evaluation participants. The Mark IIA system consists of: a computer, foam flow meter, solution flow meter, foam control valve, self-contained digital read-out unit, and associated wiring and electrical connectors. A follow-on test phase replaced the paddle wheel flow meters for water and AFFF with magnetic flow meters. The advantages of the magnetic flow meters are more consistent metering and higher maintenance reliability. The

Mark IIA computer program has been modified to meet current USAF objectives to provide foam in concentrates of 1%, 3%, and 6% at flow rates between 60 and 750 gallons per minute (GPM). The AFFF dispensing ratio of the Mark IIA system is switch selectable over a range of 0-6% AFFF by the operator from the cab of the vehicle. When the AFFF reservoir is refilled with foam concentrate, the vehicle operator can adjust the Mark IIA to match the AFFF concentration in the reservoir.

1.4 <u>TEST FORCE, LOCATION, DATES</u>. Wright Laboratory, Airbase Fire Protection and Crash Rescue Systems Section (FIVCF), managed this product evaluation to verify metering accuracy, operational effectiveness, and suitability of the Mark IIA. The initial evaluation was conducted by the Responsible Test Organization (RTO), WL/FIVCF, between 16 December 1992 and 25 June 1993, at Tyndall AFB, FL. The follow-on evaluation of the magnetic flow meters was conducted between 7 and 9 November 1994.

## SECTION II PRODUCT EVALUATION DESCRIPTION

- 2.0 <u>OBJECTIVES</u>. WL/FIVCF used the data collected to compare the AFFF metering accuracy of the Mark IIA with the orifice plate system currently employed on the P-19. The primary objective of this evaluation was to verify the AFFF metering accuracy and consistency of the Mark IIA system in the P-19 firefighting vehicle. This evaluation assessed the Mark IIA system performance, operational effectiveness, and suitability for use with the P-19.
- 2.0.1 <u>Objective E-1</u>. Assess the Mark IIA system/P-19 integration and vehicle modification procedures.
- 2.0.2 <u>Objective E-2</u>. Assess the operational performance of the Mark IIA system installed on the P-19.
- 2.0.3 <u>Objective S-3</u>. Assess the compatibility of the Mark IIA system installed on the P-19 with firefighting operations.
- 2.0.4 <u>Objective S-4</u>. Assess the adequacy of technical data provided with the Mark IIA system.
- 2.0.5 Objective S-5. Assess the Mark IIA system Reliability, Maintainability and Availability (RM&A).
- 2.1 SCOPE AND METHOD OF ACCOMPLISHMENT. Prior to modifying the P-19 vehicle with the Mark IIA system, the RTO demonstrated the AFFF metering accuracy of the existing orifice plate system for 1%, 3% and 6% AFFF. The performance baseline was established for comparison with the Mark IIA system. After the orifice plate system was baselined, the Mark IIA system was installed on the same P-19 vehicle and the same AFFF metering accuracy data was collected. At the conclusion of each foam percentage evaluations, the AFFF metering accuracies were measured using sight gauges to evaluate the repeatability of the Mark IIA system to consistently provide 1%, 3%, and 6% AFFF. When the magnetic flow meters were installed, their performance was verified by an in-line mechanical measuring meter.

The evaluation participants from FIVCF/ARA were task qualified firefighting and maintenance personnel. General firefighting practices and procedures as outlined in National Fire Protection Association Standard 412, Evaluating Aircraft Rescue and Foam Fire Fighting Equipment, were followed.

Mark IIA system reliability data are reported as mature system point data since the system is commercially available (off-the-shelf).

2.2 PLANNING CONSIDERATIONS AND LIMITING FACTORS. Only one A/S32P-19 Crash Fire Rescue Vehicle was modified for this test. The baseline metering performance of the P-19 examined 1%, 3% and 6% AFFF dispensing; however, manufactured orifice plates were available only for 3% and 6%. Former attempts to meter at 1% using an orifice plate were unsuccessful. For this test, WL/FIVCF//ARA fabricated a 1% orifice plate to establish a baseline for evaluating the Mark IIA system.

The paddle wheel flow transducer in the Mark IIA system used to measure the flow of foam is accurate between a minimum of 2.7 GPM and a maximum of 81 GPM. The magnetic flow meter used in the second phase of testing measures between 0.2 and 100 GPM. This means that during the first phase of testing, when using the bumper turret only with 1% AFFF, or when using the hand line only at 1% or 3% AFFF, the mixture will be slightly inaccurate. To more reliably measure the quantities of AFFF solution used in these cases, a small auxiliary tank was installed with a more precise measurement scale. This auxiliary tank was not in place during the baseline runs with the orifice plates.

## SECTION III EFFECTIVENESS AND SUITABILITY

- 3.0 SUMMARY. The Mark IIA system was evaluated as specified in the test plan. Data on system performance, operational effectiveness and suitability were recorded as point data due to the relatively short evaluation period. The P-19 vehicle water and AFFF tanks were calibrated. The P-19 and Mark IIA systems were serviced and prepared for use in accordance with applicable technical manuals. After preparation for use, the P-19 and Mark IIA systems were operated to dispense AFFF ten times from each turret/nozzle (roof, bumper, and handline) for 60 seconds with 1%, 3%, and 6% AFFF. After each dispensing operation, the water and AFFF tank quantities were recorded using fluid sight gauges on the vehicle to determine the amounts used. This was accomplished to compute the Mark IIA system metering accuracy and to determine repeatability with the various AFFF concentrations. In the second phase (with magnetic flow meter) each turret/nozzle was operated five times each. The handline was included to determine the Mark IIA's ability to accurately meter AFFF at low flow rates. Since the dispersal pattern is primarily determined by the turret/nozzle and has been previously established, this test evaluated only the mixture of foam concentrates. No dispersal patterns were measured or pit fires extinguished. Special attention was given to the Mark IIA system performance. Nordic Systems technicians assisted FIVCF personnel during the installation and calibration of the Mark IIA system in the P-19 evaluation vehicle. They performed a limited technical inspection (LTI) and functionally operated the Mark IIA modification prior to beginning the evaluation. FIVCF/ARA/BDM personnel compared the installed hardware and components to the technical data package provided by Nordic Systems Inc. to verify completeness. During initial test and calibration, the measurement accuracy for small quantities of foam was inconsistent. On 8 Mar 93, an auxiliary 10-gallon foam tank was added to the P-19 to provide a more precise measurement container for low foam rate delivery test events.
- **3.1** Objective E-1. Assess the Mark IIA system/P-19 integration and vehicle modification procedures.
- **3.1.1** <u>Method.</u> Nordic Systems technicians assisted FIVCF personnel in the installation and calibration of the Mark IIA system in the P-19 evaluation vehicle. They performed a limited technical inspection (LTI) and functionally operated the Mark IIA modification prior to beginning the evaluation. Nordic gathered performance data and modified the Mark IIA computer program to conform with the exhibited characteristics of the P-19 installation. FIVCF/ARA/BDM personnel compared the installed hardware and components to the technical data package provided by Nordic Systems Inc. to verify completeness.
- **3.1.2** Results and Conclusions. During the installation, pictured in Appendix C, some adjustments to the data package were necessary to reflect the actual parts and location of items on this model of the P-19. The computer metering program had to be updated once calibration runs were accomplished. The final data package accurately represents the procedures and techniques required to modify the P-19 with the Nordic Systems Inc. Mark IIA Computerized Foam Proportioning System.

- **3.1.3 Recommendations.** None.
- **3.2** Objective E-2. Assess the operational performance of the Mark IIA system installed on the P-19.
- 3.2.1 Method. The P-19 vehicle water and AFFF tanks were calibrated following the Firefighting Vehicle Fluid Calibration Procedures in the test plan. The P-19 and Mark IIA systems were serviced and prepared for use in accordance with applicable technical manuals. The P-19 and Mark IIA systems were operated to dispense AFFF ten times from each turret/nozzle (roof, bumper, and handline) for 60 seconds with 1%, 3%, and 6% AFFF. After each dispensing operation, the water and AFFF tank quantities were recorded from fluid sight gauges on the vehicle to determine the amounts used. These readings were used to compute the Mark IIA system metering accuracy and repeatability with the various AFFF concentrations. The handline was included to determine the Mark IIA's accuracy at low flow rates. During dispensing operations, special attention was given to the Mark IIA system performance.
- 3.2.2 Results and Conclusions. The Mark IIA system on the P-19 fire truck performed excellently during all phases of the evaluation. Consistent performance was difficult at the low foam flow rates. More consistent measurements were achieved using the magnetic flow meters. Metering results are summarized in Table 1 and elaborated in Figures 1 through 3. When the magnetic flow meters were installed for the second phase, the computer control had to be modified, but time and field equipment did not allow optimizing the control system. The mixture was slightly rich for all magnetic flow meter performance. In the graphs of figures 1 through 3, the left group of results are for the baseline runs, the center group is the NORDIC IIA system with paddlewheel flow meters and the right hand group is performance with the magnetic flow meters. Operationally, when the foam tank is refilled with foam of a different concentration than had been previously dispensed, the ratio of foam dispensed can be changed from inside the vehicle cab by a single switch change, providing a real time read-out of foam concentration being delivered at the dispensing nozzle. Currently a change in foam concentration requires a change in the orifice plate, a nominal 1.5 hour procedure.
- **3.2.3** Recommendations. An accurate calibration of all components in a kit should be accomplished at the production facility. If recalibration is necessary after repair actions in the field, a procedure should be incorporated in the technical order.

Table 1
Average AFFF metering system performance

	1% AFFF	3% AFFF	6% AFFF
*	0.9 - 1.2	2.8 - 3.5	5.5 - 7.0
Target Range		(2.8 - 4.0 Handline)	(5.5 - 8.0 Handline)
ROOF			
Baseline	1.1	3.8	6.7
Mark IIA	1.0	3.1	6.4
Magnetic Flow Meters	1.1	3.3	6.2
ROOF & BUMPER			
Baseline	1.1	3.8	6.5
Mark IIA	0.9	3.1	6.1
Magnetic Flow Meters	1.1	3.2	6.0
BUMPER			
Baseline	0.9	2.9	6.7
Mark IIA	1.2	2.7	6.0
Magnetic Flow Meters	1.2	3.5	6.8
HANDLINE			
Baseline	1.1	3.7	5.2
Mark IIA	1.7	2.8	5.9
Magnetic Flow Meters	2.1	3.6	6.8

Target ranges for 3% and 6% AFFF have been established in NFPA Standard 412, the target range for 1% has not been established by NFPA but was introduced by applying criteria similar to the 3% and 6% ranges.

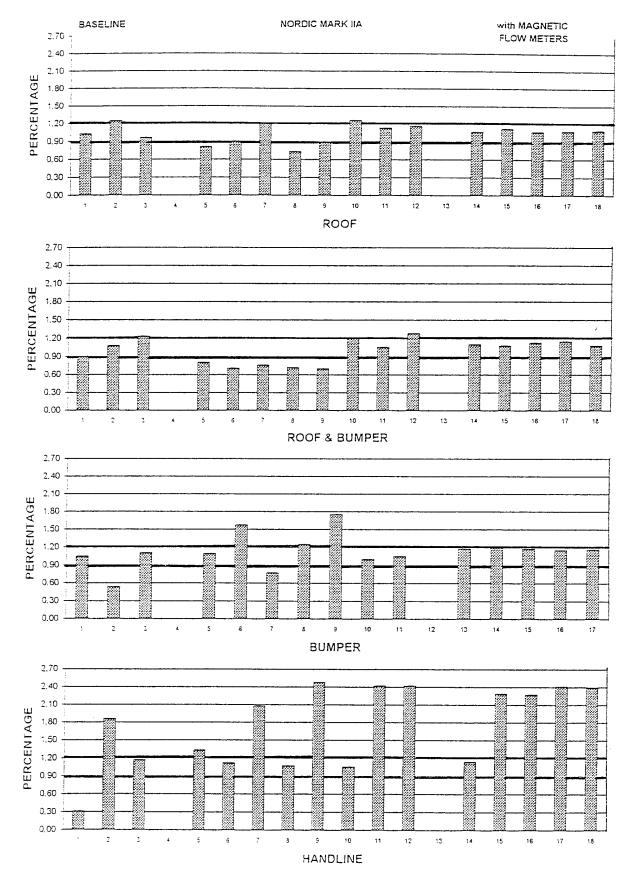


Figure 1 1% AFFF Performance Target Range 0.9 - 1.2%

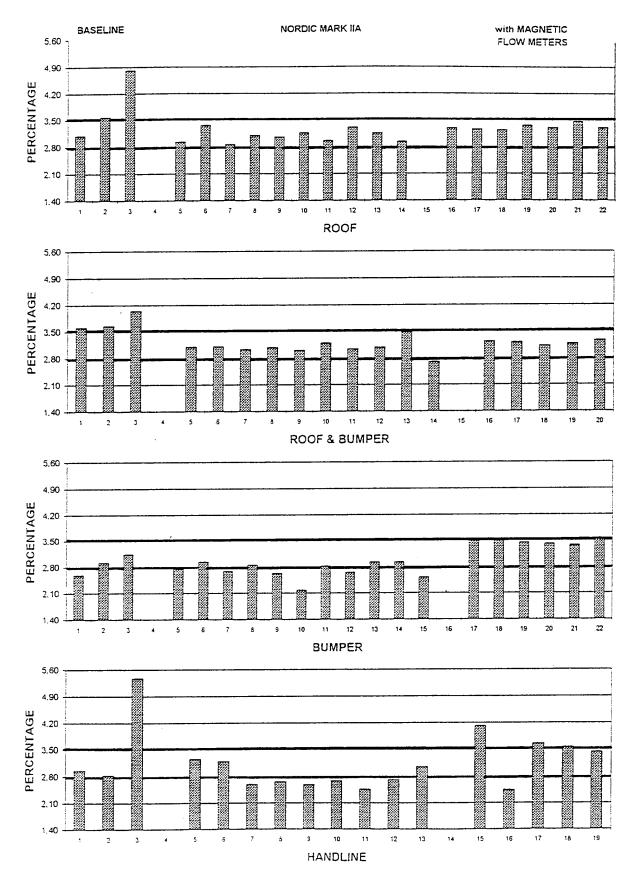


Figure 2 .
3% AFFF Performance
Target Range 2.8 - 3.5%

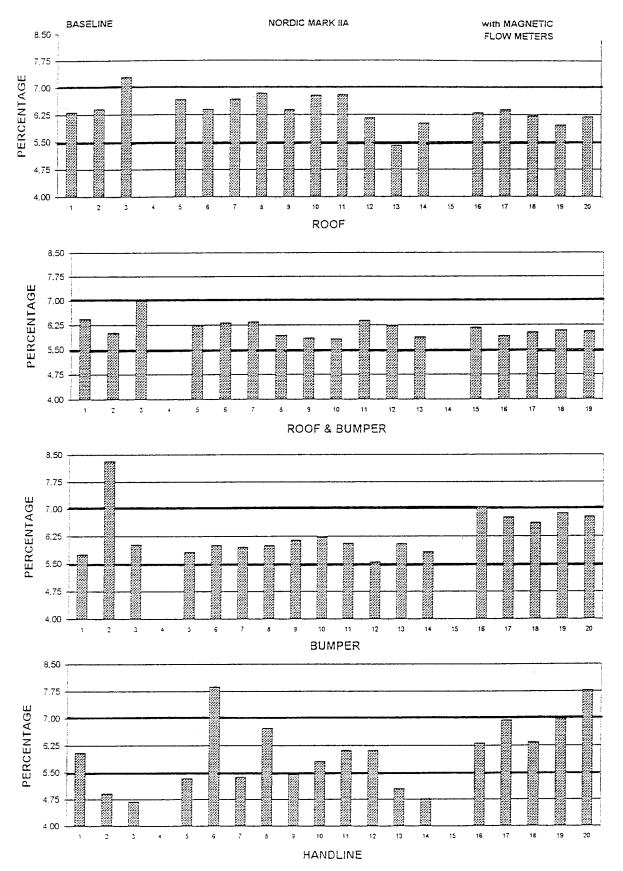


Figure 3 6% AFFF Performance Target Range 5.5 - 7.0%

- **3.3** Objective S-3. Assess the compatibility of the Mark IIA system with the P-19 firefighting vehicle.
- **3.3.1** Method. The Mark IIA system was employed as described in the test plan and maintained IAW the operational concept and the manufacturer's technical data. The evaluation participants were briefed to be alert for any actual or foreseeable compatibility problems between and among the components and to notify the Evaluation Manager of any observed or experienced compatibility problems.
- **3.3.2** Results and Conclusions. No incompatibilities between the Mark IIA system and the P-19 fire truck were noted. Once the system was installed, changing to a different foam concentration required a single switch change instead of the nominal 1.5 hours previously required to change orifice plates. From a firefighters perspective, operations using the metering system were transparent to using the orifice plate system. With this type of metering system installed, the P-19 becomes more versatile due to its expanded capability to operate using 1% foam concentrate. The addition of this system makes the Air Force A/S32P-19 Crash Fire Rescue Vehicle or any other fire vehicle better suited for worldwide contingency operations using stockpiles of differing foam concentrations.
- **3.3.3** <u>Recommendations</u>. Investigate retrofit installation of a computerized metering system on all Air Force Fire/Crash Rescue vehicles that use AFFF as their primary firefighting agent.
- **3.4** Objective S-4. Assess the adequacy of the vendor provided technical manuals for the Mark IIA system.
- **3.4.1** <u>Method</u>. During this evaluation, participants used the vendor provided technical manuals. After each evaluation event, the participants indicated, on data forms and maintenance logs, any difficulties that prevented or hindered successful task performance. The Evaluation Manager recorded pertinent observations and comments in the Evaluation Manager's Log. The technical manual was reviewed and verified.
- **3.4.2** Results and Conclusions. During the installation, some adjustments to the data package were necessary to reflect the actual parts and location of items on this model of the P-19. The final data package accurately represents the procedures and techniques required. Operating instructions for the Nordic Systems Inc. Mark IIA Computerized Foam Proportioning System were clear and adequate for the necessary control settings and adjustments.
- **3.4.3** Recommendations. The next kit installed should serve as a kit proofing to verify that the data package is appropriate for base or depot level modification, depending upon where system installations will be accomplished.

- **3.5** Objective S-5. Assess the Mark IIA system Reliability, Maintainability, and Availability (RM&A).
- **3.5.1** <u>Method.</u> The Evaluation Manager and participants recorded any system failures and repair data. These data were to serve as the basis to calculate system point RM&A rates for the evaluation period.
- 3.5.2 Results and Conclusions. After the magnetic flow meters were installed, the computer controlled foam metering valve was operating erratically. The valve was replaced to provide accurate test results. This component was a manual valve that the contractor (NORDIC) had modified to be controlled by an electric motor. Since that phase of testing, the valve has been replaced by a commercially produced motorized valve made by Elkart. No system failures occurred during the evaluation period and no repairs were required. The first phase of test consisted of 32 hours of operation. The vehicle was in use for 16 months between phases and the system accumulated 56 hours of test operation by the conclusion of testing. This length of documented test operation is inadequate to provide any long term RM&A data. Mean Time Between Maintenance (MTBM) and Mean Down Time (MDT) could not be calculated since no records account for the amount of use during the 16 months between test phases. Operational Availability (Ao) was 100% during the periods of this evaluation.
- **3.5.3** <u>Recommendations</u>. If representative RM&A data are required, recommend a number of systems be installed in operational units and operated for a minimum of six months.

## SECTION IV SUMMARY OF CONCLUSIONS AND RECOMMENDATIONS

- **4.0 Conclusions.** During the installation, some adjustments had to be made to the plumbing and data package. The final data package outlines the requirements to modify the P-19 with the Mark IIA System. Consistent performance was difficult at the low foam flow rates. More consistent measurements were achieved by using magnetic flow meters. When the foam tank is refilled with foam of a different concentration than has been previously dispensed, the ratio of foam dispensed can be changed from inside the vehicle by a single switch change instead of the nominal 1.5 hours previously required to change orifice plates. A real time read-out of foam dispensing concentration is presented to the operator. No incompatibilities between the Mark IIA system and the P-19 fire truck were noted. From a firefighters perspective, operations using the metering system were transparent to using the orifice plate system. With this type of metering system installed, the P-19 becomes more versatile due to its expanded capability to operate using 1%, 3% and 6% foam concentrate. The addition of this system makes Air Force Crash Fire Rescue Vehicles better suited for worldwide contingency operations. Operating instructions for the Mark IIA were clear and adequate for the necessary control settings and adjustments. No system failures occurred during the evaluation period and no repairs were required. The test events, completed during 56 hour of operation, were inadequate to provide any long term RM&A data. Operational Availability (Ao) was 100% during the period of this evaluation.
- **4.1** Recommendations. Recommend that a computerized foam metering system be competitively procured for field and/or depot retrofit of P-19, P-23, and other front line ARFF vehicles. If a system calibration is required after field level repair, a procedure should be added to the technical order. If representative RM&A data is required, recommend a number of systems be installed in operational units and operated for a minimum of six months.

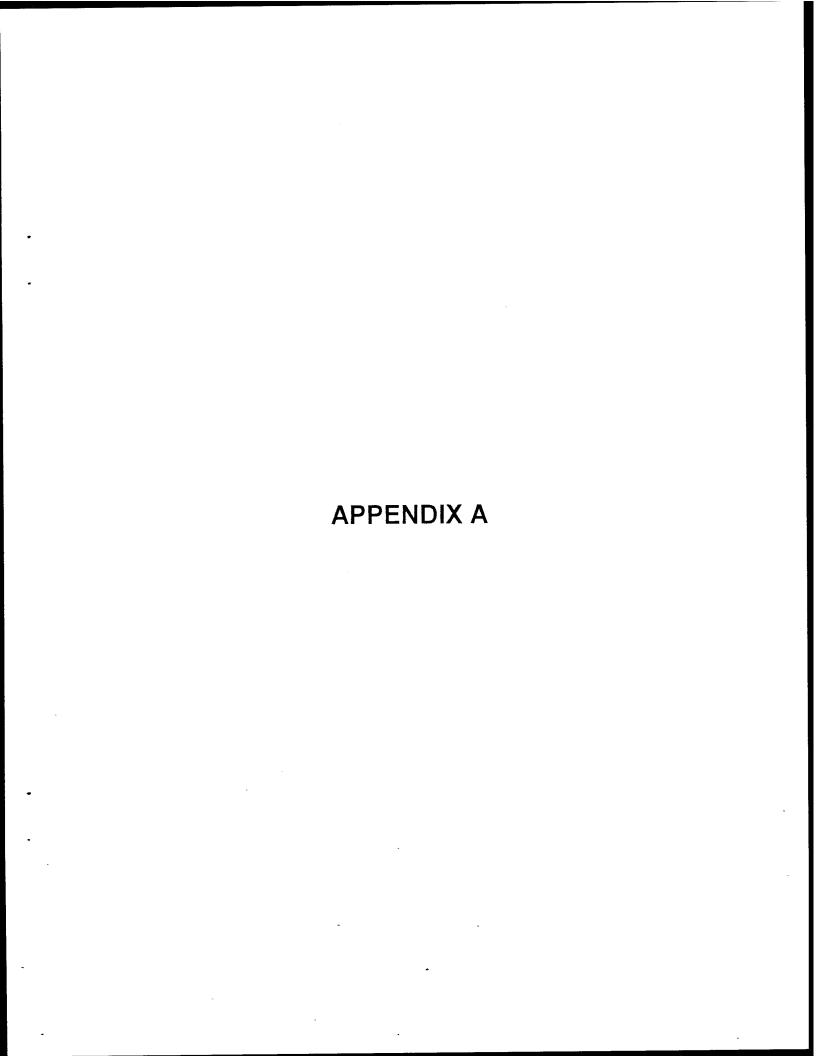


Table A-1 P-19 fluid tank calibration table

Wate	er Tank	Fill	AFF	Tank	Auxiliary	AFFF Tank
Quantity Gallons	Depth in inches	Point	Quantity Gallons	Depth in inches	Quantity Gallons	Depth in inches
0	8	1	0	19	0	0
50	10 1/2	2	5	21 1/16	1	2 15/16
100	12 5/16	3	10	22 3/8	2	5 7/8
150	15 5/16	4	15	23 9/16	3	8 13/16
200	17 5/8	5	20	24 3/16	4	11 3/4
250	20	6	25	24 15/16	5	14 11/16
300	22 3/16	7	30	25 5/8	6	17 5/8
350	23 15/16	8	35	26 5/16	7	20 19/32
400	25 1/2	9	40	27 1/8	8	23 17/32
450	27 3/16	10	45	27 15/16	9	26 15/32
500	28 7/8	11	50	28 5/8	10	29 13/32
550	30 9/16	12	55	29 5/8	11	32 11/32
600	32 1/4	13	60	29 15/16	12	35 9/32
650	33 15/16	14	65	30 5/8		
700	35 9/16	15	70	31 3/8		
750	37 5/16	16	75	32		
800	39	17	80	32 5/8		
850	40 5/8	18	85	33 3/8		
900	42 1/4	19	90	34 1/16		
950	43 15/16	20	95	34 3/4		
1000	45 5/8	21	100	35 3/8		
		22	105	36 1/8		
		23	110	36 3/4		
		24	115	37 9/16		
		25	120	38 1/8		
		26	125	38 7/8	_	
		27	130	39 13/16		

## APPENDIX A NORDIC MARK IIA EVALUATION MATRIX AND RESULTS

			,									TABILI			1	CALC.
FIGURE				PLANNED	ACTUAL	INC		R TANK	LONS	INI	CHES	TANK GAL	LONS	WATER	AFFF	RATIO
GRAPH NO.	TEST NO.	TURRET	AFFF TANK	DISPENSING TIME (sec)	DISPENSING TIME (sec)	START	END	START	END	START	END	START	END	USED	USED	<b>≈</b>
1-1	R 1-1	ROOF	AFFF	60	60.1	45.688	27.188	1001.370	450.000	31.625	30.813	72.000	66.250	551.370	5.750	1.03
1.2	R 2-1	ROOF	AFFF	60	60.2	32.531	8.938	608.333	18.750	30.063	29.313	60.909	53.438	589.583	7.472	1.25
1.3	R 3-1	ROOF	AFFF	60	60.2	45.688	29.313	1001.370	512.963	29.125	28.313	52.500	47.727	488.407	4.773	0.97
1.5	7	ROOF	AFFF	60	60.1	32.813	12.125	616.667	83.333	28.219	27.563	47.045	42.694	533.333	4.351	0.81
1-6	. 9	ROOF	AFFF	. 60	60.1	45.625	28.000	1000.000	474.074	26.500	25.813	36.154 24.169	31.365 17.752	525.926 522.222	4.789 6.417	0.90 1.21
1-7	- 14	ROOF	AFFF	60	60.2 60.1	43.438 45.531	25.938 28.156	935.185 997.222	412.963 478.704	24.813	26.688	41.155	37.308	518.519	3.847	0.74
1-8	16	ROOF	AFFF	. 80	60.5	45.625	28.094	1000.000	476.852	26.344	25.688	35.192	30.455	523.148	4.737	0.90
1-10	23	ROOF	AFFF	60	59.9	41.344	24.000	872.115	352.000	25.094	24.125	26.136	19.504	520.115	6.633	1.26
1-11	25	ROOF	AFFF	60	<b>60</b> .0	45.594	28.000	999.074	474.074	25.594	24.750	29.773	23.753	525.000	6.020	1.13
1-12	29	ROOF	AFFF	60	60.0	<b>45.62</b> 5	28.188	1000.000	479.630	26.156	25.313	33.866	27.727	520.370	6.139	3.10
2-1	R 1-3	ROOF	AFFF	60	60.0	45.688	26.500 26.188	1001.370	429.630 420.370	39.875 30.625	37.063 27.688	130.204 65.000	43.464	571.740 579.630	18.280 21.536	3.58
2-2	R 2-3	ROOF	AFFF	. 60	60.2	45.625 45.688	26.344	1001.370	425.000	25.938	20.313	32.274	3.183	576.370	29.092	4.80
2.5	1 1	ROOF	AFFF	- 60	60.1	45.594	28.563	999.074	490.741	37.531	35.313	114.811	99.500	508.333	15.311	2.92
2.6	4/2	ROOF	AFFF	60	60.0	45.625	28.438	1000.000	487.037	34.250	31.813	91.364	73.500	512.963	17.864	3.37
2.7	4/3	ROOF	AFFF	60	60.2	32.875	12.750	618.519	96.154	39.563	37.281	128.669	113.271	522.365	15.397	2.86
2.8	55	ROOF	AFFF	60	65.0	45.625	26.313	1000.000	424.074	37.344	34.781	113.656	95.250 112.886	575.926 505.556	18.406 15.949	3.10
2.9	6	ROOF	AFFF	<u></u>	60.0 60.2	45.438 36.938	28.500 18.625	739.286	488.889 221.053	39.594 38.531	37.219 36.219	128.835 122.708	105.750	518.233	16.958	3.17
2.10	13/2	ROOF	AFFF	60	60.1	45.594	28.375	999.074	485.185	39.469	37.156	128.168	112.502	513.889	15.667	2.96
2.12	13/3	ROOF	AFFF	60	60.1	45.625	28.406	1000.000	486.111	33.969	31.594	89.321	71.750	513.889	17.571	3.31
2-13	18	ROOF	AFFF	60	60.3	43.344	26.281	932.407	423.148	36.094	33.813	104.792	88.184	509.259	16.608	3.16
2-14	20	ROOF	AFFF	60	60.1	45.625	28.469	1000.000	487.963	39.688	37.375	129.336 127.168	90.682	512.037 541.185	15.487 36.486	6.32
3-1	R 1-6	ROOF	AFFF	- 60	60.0	45.688	27.531	1001.370	460.185 444.444	39.281 31.625	34.156 26.156	72.000	33.866	556.925	38.134	6.41
3-2	R 2-6	ROOF	AFFF	<u>60</u>	<u>60.2</u> 60.0	45.688 45.688	27.563	1001.370	461.111	36.375	30.563	107.000	64.545	540.259	42.455	7.29
3-5	1 1	ROOF	AFFF	60	60.1	45.500	28.875	996.296	500.000	39.719	34.625	129.502	94.091	496.296	35.411	6.66
3-6	5	ROOF	AFFF	60	60.0	43.406	26.688	934.259	435.185	39.219	34.438	126.834	92.727	499.074	34.107	6.40
3-7	8	ROOF	AFFF	60	60.0	43.500	26.969	937.037	443.519	39.312 39.188	34.344 34.094	127.335 126.668	92.045	493.519 496.296	35.289 36.440	6.84
3-8	13	ROOF	WATER	60	<u>60.1</u> 59.8	45.500 45.625	28.875 29.094	996.296	500.000 506.481	39.563	34.750	128.669	95.000	493.519	33.669	6.39
3-10	15	ROOF	AFFF	60	60.0	45.625	28.906	1000.000	500.926	39.375	34.250	127.668	91.364	499.074	36.304	6.78
3-11	19	ROOF	AFFF	. 60	60.3	45.500	28.938	996.296	501.852	39.375	34.281	127.668	91.591	494,444	36.077	6.80
3-12	34	ROOF	WATER	60	60.0	45.625	29.031	1000.000	504.630	39.000	34.500	125.667	93.182	495.370	32.485	6.15
3-13	35	ROOF	WATER	60	60.0	45.625	27.063 28.875	996.296	446.296 500.000	39.563 39.125	35.000 34.688	128.669 126.334	97.000 94.545	553.704 496.296	31.669	6.02
3-14	36 R8 1-1	ROOF/BUMP	AFFF	60	60.2 60.3	45.500 45.688	18.188	1001.370	211.842	27.969	26.813	45.227	38.077	789.528	7.150	0.90
1.2	RB 2-1	ROOF/BUMP	AFFF		60.1	45.688	18.875	1001.370	226,316	26.875	25.625	38.462	30.000	775.054	8.462	1.08
1-3	RB 3-1	ROOF/BUMP	AFFF	60	60.0	45.688	19.000	1001.370	228.947	25.750	24.375	30.910	21.251	772.422	9.659	1.24
1.5	3	ROOF/BUMP	AFFF	60	60.0	45.500	18.250	996.296	213.158	28.813	27.875	50.938	44.618	783.138	6.319	0.80
1-6	4	ROOF/BUMP	AFFF	. 60	60.1	45.594	18.219	999.074 998.148	212.500 205.263	27.906 27.000	27.000 26.063	44.811 39.231	39.231 33.184	786.574 792.885	5.580 6.047	0.76
1-7	5	ROOF/BUMP	AFFF	. <u>6</u> 0 60	60.0 60.0	45.563 45.625	17.875	1000.000	207.895	28.250	27.375	47.273	41.539	792.105	5.733	0.72
1.9	8	ROOF/BUMP	AFFF	60	60.0	45.625	18.000	1000.000	207.895	27.375	26.469	41.539	35.962	792.105	5.578	0.70
1-10	30	ROOF/BUMP	AFFF	60	60.1	45.344	17.750	991.667	202.632	25.375	24.000	28.182	18.503	789.035	9.679	1.21
1-11	31	ROOF/BUMP	AFFF	. 60	60.1	14.594	16.750	969.444	181.081	26.125	24.969	33.639	25.227 14.607	788.363 783.258	8.412 10.188	1.06
1-12	32	ROOF/BUMP	AFFF	60	60.0	44.969	17.500	980.556 1000.000	197.297	24.906 35.313	23.469 31.156	24.795 99. <b>50</b> 0	68.542	825.676	30.958	3.61
2-1	RB 1-3 RB 2-3		AFFF	60 60	60.1 60.0	45.625 45.688	16.438	1001.370	174.324	33.563	29.625	86.365	55.000	827.046	31.365	3.65
2-3	RB 3-3		AFFF	60	60.1	45.250	17.875	988.889	205.263	27.750	22.563	43.849	10.790	783.626	33.059	4.05
2-5	9	ROOF/BUMP	AFFF	60	<b>60</b> .0	45.531	18.563	997.222	219.737	36.188	32.719	105.500	80.625	777.485	24.875	3.10
2-6	10/2	ROOF/BUMP	AFFF		60.3	45,500	19.094	996.296	230.921	36.281	32.875	106.250 128.502	81.667 104.375	765.375 771.296	24.583 24.127	3.11
2-7	10/3	ROOF/BUMP	AFFF	. 60	60.0 60.1	45.500 45.594	18.813	996.296 999.074	225.000 229.605	39.531 38.656	36.031 35.250	128.502	99.000	769.469	24.127	3.09
2-8 2-9	11/2 11/3	ROOF/BUMP	AFFF	. 60 60	60.2	45.594	18.625	999.074	221.053	36.031	32.656	104.375	80.208	778.021	24.167	3.01
2-10	12/2	ROOF/BUMP	AFFF	90 90	60.0	45.594	18.625	999.074	221.053	35.281	31.813	99.250	73.500	778.021	25.750	3.20
2-11	12/3	ROOF/BUMP	AFFF	60	59.9	45.594	18.844	999.074	225.658	37.406	34.031	114.041	89.776	773.416	24.265	3.04
2-12	22	ROOF/BUMP	AFFF	60	60.0	45.625	19.125	1000.000	231.579	36.375	33.000	107.000	82.500	768.421	24.500 28.021	3.09 3.50
2.13	23	ROOF/BUMP	AFFF	. 60	60.0 .60.1	45.625	18.875 18.844	990.741	226.316 225.658	33.031 29.563	29.563 26.094	<b>82.708</b> <b>54.68</b> 8	54.688 33.412	773.684 765.083	28.021	2.71
3-1	24 RB 1-6	ROOF/BUMP	AFFF	60	60.3	45.313 45.000	15.313	981.481	150.000	30.438	21.438	63.636	6.429	831.481	57.208	6.44
3.2	RB 2-6		AFFF	60	60.2	45.688	16.500	1001.370	175.676	37.500	29.938	114.618	60.000	825.694	54.618	6.01
3.3	RB 3-6		AFFF	60	60.1	45.025	19.500	1000.000	239.474	31.313	22.938	69.583	12.369	760.526	57.214	7.00
3-5	10	ROOF/BUMP	AFFF	Oc	<b>59</b> .9	45.53!	19.906	997.222	248.026	39.375	32.344	127.668	77.750	749.196	49,918	6.25
3-6	11	ROOF/BUMP	AFFF	50	60.0 40.0	45.625	20.000	1000.000	250.000	39.500	32,344	128.335 128.335	77.750 77.744	750.000 747.344	50.585 50.591	5.32 6.34
3-7	12 13	ROOF/BUMP	AFFF WATER	ა0 ა0	50.0 60.1	45.46 <sup>3</sup> 45.525	19.906 19.563	995.370	248.026 240.789	39.500 39.563	32.343 32.750	128.669	80.833	759.211	47.835	5.93
3.8	.3	ROOF/BUMP	WATER	50 50	50.1	45.625	19.813	1000.000	246.053	39.688	33.000	129.336	32.500	753.947	46.836	5.85
3-10	:5	ROOF/BUMP	WATER	50	50.2	45.625	19.562	1000.000	240.779	39.625	32.938	129.002	<b>82</b> .083	759.221	46.919	5.82
3-11	22	ROOF/BUMP	AFFF	50	<b>50</b> .0	45.625	20.188	1000.000	254.286	39.500	32.313	128.335	77.500	745.714	50.835	6.38
3-12	23	ROOF/BUMP	AFFF	50	50.1	45.525	20.125	1000.000	252.857	36.000	29.563	104.167	54.688	747,143	49.479	6.21 5.88
3.13	24	ROOF/BUMP	AFFF	50	5 <b>0</b> .0	<b>45</b> .500	24.250	796.296	360.000	29.813	23.969	58.005	18.253	5 <b>36</b> .296	39.752	.5.00



### ND RESULTS

	ACEC	TANK		1	Γ	CALC.	TARGET		FLOW		T	AFFF NO	D CYLINI	DER
INC	CHES		LLONS	WATER	AFFF	RATIO	RATIO	ERROR	RATE	AMB.	TEST		CHES	<u> </u>
TART	END	START	END	USED	USED	%	%	%	(GPM)	TEMP	DATE	START	END	5
.625	30.813	72.000	66.250	551.370	5.750	1.03	1	0.03	556.2	56	18-Dec-92			
0.063	29.313	60.909	53.438	589.583	7.472	1.25	! .	0.25	595.1	58	18-Dec-92			
2.125	28.313	52.500	47.727	488.407	4.773	0.97	1	-0.03 -0.19	491.5 536.8	65 	18-Dec-92 23-Jun-93			
3.219 3.500	27.563 25.813	47.045 36.154	42.694 31.365	533.333 525.926	4.351	0.90	1	-0.19	529.8	80	24-Jun-93			
1.813	23.906	24.169	17.752	522.222	6.417	1.21	1	0.21	526.9	81	24-Jun-93			
7.313	26.688	41.155	37.308	518.519	3.847	0.74	1	-0.26	521.5	82	24-Jun-93			
.344	25.688	35.192	30.455	523.148	4.737	0.90	11	-0.10	523.5	83	24-Jun-93			
.094	24.125	26.136	19.504	520.115	6.633	1.26		0.26	527.6	83	24-Jun-93			
5.594	24.750	29.773	23.753	525.000	6.020	1.13	1	0.13	531.0 526.5	84	24-Jun-93 20-May-93			
.156 .875	37.063	33.866 130.204	27.727	520.370 571.740	18.280	3.10	3	0.03	590.0	74	16-Dec-92			
.625	27.688	65.000	43.464	579.630	21.536	3.58	3	0.19	599.2	74	16-Dec-92			
.938	20.313	32.274	3.183	576.370	29.092	4.80	3	0.60	603.5	69	17-Dec-92			
.531	35.313	114.811	99.500	508.333	15.311	2.92	3	-0.03	522.8	_85	22-Jun-93			
.250	31.813	91.364	73.500	512.963	17.864	3.37	3	0.12	530.8	85	22-Jun-93	0.000	0.000	
.563	37.281	128.669	113.271	522.365	15.397	2.86 3.10	<u>3</u>	-0.05 0.03	536.0 548.6	82 82	23-Jun-93 23-Jun-93	0.002	0.002	
.344	34.781 37.219	113.656 128.835	95.250 112.886	575.926 505.556	18.406	3.06	3	0.03	521.5	86	22-Jun-93			
1.531	36.219	122.708	105.750	518.233	16.958	3.17	3	0.06	533.4	83	23-Jun-93			
.469	37.156	128.168	112.502	513.889	15.667	2.96	3	-0.01	528.7	83	22-Jun-93			
.969	31.594	89.321	71.750	513.889	17.571	3.31	3	0.10	530.6	86_	23-Jun-93			
.094	33.813	104.792	88.184	509.259	16.608 15.487	3.16 2.94	3	0.05 -0.02	523.3 526.6	<u>82</u> 82	22-Jun-93 22-Jun-93			
.688	37.375 34.156	127.168	90.682	512.037 541.185	36.486	6.32		0.02	577.7	72	17-Dec-92			
625	26.156	72.000	33.866	556.925	38.134	6.41	6	0.07	593.1	72	17-Dec-92			
.375	30.563	107.000	64.545	540.259	42.455	7.29	6	0.21	582.7	72	17-Dec-92			
719	34.625	129.502	94.091	496.296	35.411	6.66	66	0.11	530.8	78	25-Jun-93			
.219	34.438	126.834	92.727	499.074	34.107	6.40	6	0.07	533.2	83	25-Jun-93			
.312	34.344 34.094	127.335 126.668	92.045	493.519 496.296	35.289 36.440	6.67 6.84	6	0.11	528.8 531.9	83 84	25-Jun-93 25-Jun-93			
1.563	34.750	128.669	95.000	493.519	33.669	6.39	6	0.06	529.0	<del>7</del> 0	10-Mar-93	35.250	35.25	
.375	34.250	127.668	91.364	499.074	36.304	6.78	6	0.13	535.4	84	25-Jun-93			
.375	34.281	127.668	91.591	494.444	36.077	6.80	6	0.13	527.9	84	25-Jun-93			
.000	34.500	125.667	93.182	495.370	32.485	6.15		0.03	527.9	81	19-May-93	28.688	28.68	
.563 .125	35.000 34.688	128.669	97.000	553.704 496.296	31.669	6.02	6	-0.10 0.00	585.4 526.3	81 80	19-May-93 19-May-93	28.688	28.68	
.969	26.813	45.227	38.077	789.528	7.150	0.90	1	-0.10	792.7	66	18-Dec-92			$\dashv$
.875	25.625	38.462	30.000	775.054	8.462	1.08	1	0.08	782.2	67	18-Dec-92			
.750	24.375	30.910	21.251	772.422	9.659	1.24	1	0.24	782.1	-68	18-Dec-92			
.813	27.875	50.938	44.618	783.138	6.319	0.80 0.70	1 -	-0.20 -0.30	789.5 790.8	78 78	24-Jun-93 24-Jun-93			
.906 .000	27.000 26.063	44.811 39.231	39.231 33.184	786.574 792.885	5.580	0.76	<del></del>	-0.24	798.9	79	24-Jun-93			
.250	27.375	47.273	41.539	792.105	5.733	0.72	1	-0.28	797.8	79	24-Jun-93			
.375	26.469	41.539	35.962	792.105	5.578	0.70	1	-0.30	797.7	79	24-Jun-93			_
.375	24.000	28.182	18.503	789.035	9.679	1.21		0.21	797.4	86	24-Jun-93			
.125 .906	24.969	33.639 24.795	25.227 14.607	788.363 783.258	8.412 10.188	1.06	<u> </u>	0.06	795.4 793.4	_ <del>87</del>	24-Jun-93 24-Jun-93			
.313	31.156	99.500	68.542	825.676	30.958	3.61	3	0.20	855.2	74	16-Dec-92			$\neg$
563	29.625	86.365	55.000	827.046	31.365	3.65	3	0.22	858.4	69	17-Dec-92			
750	22.563	43.849	10.790	783.626	33.059	4.05	3	0.35	815.3	69	17-Dec-92			
188	32.719	105.500	80.625	777.485	24.875	3.10	3	0.03	802.4	83	23-Jun-93			
.281 531	32.875	106.250 128.502	81.667 104.375	765.375 771.296	24.583 24.127	3.11	3	0.04	786.0 795.4	86 83	22-Jun-93 23-Jun-93			
.5 <u>31</u> .656	36.031 35.250	123.542	99.000	769.469	24.542	3.09	3 -	0.03	792.7	83 84	22-Jun-93			
031	32.656	104.375	80.208	778.021	24.167	3.01	3	0.00	799.5	84	23-Jun-93			
281	31.813	99.250	73.500	778.021	25.750	3.20	3	0.07	803.8	84	22-Jun-93			
406	34.031	114.041	89.776	773.416	24.265	3.04	3	0.01	799.0	84	23-Jun-93			
375 031	33.000	107.000	82.500 54.688	768.421 773.684	24.500 28.021	3.09	3 3	0.03	792.9 801.7	82 	22-Jun-93 22-Jun-93			
<b>0</b> 31 <b>5</b> 63	29.563 26.094	82.708 54.688	33.412	765.083	28.021	3.50 2.71	3 3	-0.10	785.1	82	22-Jun-93			]
438	21.438	63.636	6.429	831.481	57.208	6.44	6	0.07	884.3		18-Dec-92	-		$\neg$
<b>5</b> 00	29.938	114.618	60.000	825.694	54.618	6.01	. 0	0.00	877.4	50	18-Dec-92			1
313	22.938	69.583	12.369	760.526	57.214	7.00	6	0.17	816.4		18-Dec 92			ļ
375 500	32.344	127.668	77.750	749,196	49.918	6.25	5 .	0.04	800.4	_83 _84	25-Jun-93 25-Jun-93			ŀ
<b>50</b> 0 <b>5</b> 00	32.344 32.343	128.335 128.335	77.750 77.744	750.000 747.344	50.585 50.591	6.32 6.34	ó .	0.05 0.06	800.6 797.9	84 84	25-Jun-93			1
563	32.750	128.669	80.833	759.211	47.835	5.93	0	0.00	805.7		19-May-93			
<b>688</b>	33.000	129.336	82.500	753.947	46.836	5.85	5	-0.03	799.5		19-May-93			
<b>6</b> 25	32.938	129.002	82.083	759.221	46.919	5.82	2	-0.03	∂03.5		19-Mav-93			1
500	32.313	128.335	77.500	745,714	50.835	5.38	5	0.06	796.5	36	25-Jun-93			
000	29.563	104.167	54.688	747,143	49.479	5.21	٥	0.04	796.6	86 84	25-uun-93			
813	23.969	58.005	18.253	აპბ.29ბ	39.752	5.88		-0.02	811.3	34	25-Jun-93			



#### APPENDIX A NORDIC MARK IIA EVALUATION MATRIX AND RESULTS

FIGURE	1	i	т —	PLANNED	ACTUAL		WATE	R TANK		1	AFF	TANK		Γ	i	CAL
GRAPH	TEST		AFFF	DISPENSING	I	IN	CHES		LONS	IN	CHES		LONS	WATER	AFFF	RAT
NO.	NO.	TURRET	TANK	TIME (sec)	TIME (sec)	START	END	START	END	START	END	START	END	USED	USED	1 %
1-1	B 1-1	BUMPER	AFFF	60	60.1	27.188	14.750	450.000	138.158	30.813	30.344	66.250	62.955	311.842	3.295	1.0
1.2	B 2-1	BUMPER	AFFF	60	60.0	23.938	12.438	350.000	89.744	29.313	29.031	53.438	52.031	260.256	1.406	0.5
1-3	B 3-1	BUMPER	AFFF	60	60.0	25.938	13.250	412.963	106.579	24.438	23.969	21.668	18.253	306.384	3.415	1.1
1-5	10	BUMPER	AFFF	60	60.0	28.000	17.937	474.074	206.568	25.813	25.406	31.365	28.409	267.495	2.956	1.0
1-6	15	BUMPER	AFFF	. 60	<b>60.</b> 0	25.938 28.156	14.969	412.963	142.763 207.895	23.906 26.688	23.188	17.752 37.308	13.422 35.192	270.200 270.809	2.115	1.5 0.7
1-8	17	BUMPER	AFFF		60.1	28.094	17.938	476.852	206.579	25.688	25.219	30.455	27.045	270.273	3.409	1.2
1-9	24	BUMPER	AFFF	60	60.0	24.000	12.188	352.000	84.615	24.125	23.500	19.504	14.739	267.385	4.765	1.7
1-10	26	BUMPER	AFFF	60	60.0	45.625	36.750	1000.000	733.929	26.906	26.469	38.654	35.962	266.071	2.692	1.0
1-11	27	BUMPER	AFFF	60	<b>60</b> .0	36.750	27.938	733.929	472.222	26.469	26.063	35.962	33.184	261.706	2.777	1.0
2-1	B 1-3	BUMPER	AFFF	60	. 60.3	26.188	12.969	420.370	100.658	27.688	26.313	43.464	35.000	319.712	8.464	2.5
2-2	B 2-3	BUMPER	AFFF	60	60.3	45.688 35.625	35.625 25.188	701.786	701.786 390.000	36.125 34.875	34.875 33.500	105.000 96.000	96.000 85.910	299.584 311.786	9.000	2.9 3.1
2-3	B 3-3	BUMPER	AFFF		60.2	28.563	18.969	490.741	228.289	35.313	34.344	99.500	92.045	262.451	7.451	2.7
2-6	3	BUMPER	AFFF	. 60	60.1	41.438	32.875	875.000	618.519	39.563	39.563	128.669	128.669	256.481	7.751	2.9
2.7	5	BUMPER	AFFF	60	60.0	28.438	18.750	487.037	223.684	31.813	30.813	73.500	66.250	263.353	7.250	2.6
2-8	6	BUMPER	AFFF	60	60.0	26.313	15.781	424.074	160.135	34.781	33.719	95.250	87.502	263.939	7.748	2.8
2-9	7/2	BUMPER	AFFF	60	60.1	28.500	18.750	488.889	223.684	37.219	36.219	112.886	105.750	265.205	7.136	2.6
2-10	7/3	BUMPER	AFFF	60	60.1	45.625	36.938	1000.000	739.286	39.531 37.156	38.531 36.094	128.502	122.708 104.792	260.714 266.112	5.794 7.710	2.1
2-11	14/2	BUMPER	AFFF.		60.0 60.0	28.375	18.531 18.625	485.185 486.111	219.074 221.053	31.594	30.563	71.750	64.545	265.058	7.710	2.6
2-13	17	BUMPER	AFFF	60	30.5	41.375	36.969	873.077	740.179	30.562	30.562	64.542	64.542	132.898	4.006	2.9.
2-14	19	BUMPER	AFFF	60	60.0	26.281	15.719	423.141	158.784	33.813	32.656	88.184	80.208	264.357	7.976	2.9
2-15	21	BUMPER	AFFF	60	60.5	28.469	18.688	487.963	222.368	37.375	36.375	113.849	107.000	265.595	6.849	2.5
3-1	B 1-6	BUMPER	AFFF	60	60.2	27.531	15.500	460.185	154.054	34.156	31.625	90.682	72.000	306.131 294.444	18.682 26.724	5.75 8.33
3-2 3-3	8 2-6 B 3-6	BUMPER	AFFF	60 60	60.1 60.0	27.000 27.563	15.313	461.111	150.000	26.156 30.563	21.625 27.875	33.866 64.545	44.618	311.111	19.927	6.0
3.5	2	BUMPER	AFFF		60.1	28.875	19.688	500.000	243.421	34.625	32.406	94.091	78.250	256.579	15.841	5.8
3-6	6	BUMPER	AFFF	60	60.0	26.688	16.750	435.185	181.081	34.438	32.188	92.727	76.500	254.104	16.227	6.00
3-7	8	BUMPER	WATER	60	60.1	29.031	19.375	504.630	236.842	34.500	32.156	93.182	76.250	267.788	16.932	5.9
3-8	- °	BUMPER	AFFF	60	60.0	26.969	17.063	443.519	187.838	34.344	32.094	92.045 97.000	75.750 79.500	255.681 267.398	16.295 17.500	5.90
3-9 3-10	10	BUMPER	WATER	<u>60</u>	60.1 60.0	29.063 28.875	19.438 19.125	505.556 500.000	238.158 231.579	35.000 34.688	32.563 32.219	94.545	76.750	268.421	17.795	6.2
3-11	15	BUMPER	AFFF		60.0	26.844	16.875	439.815	183.784	34.063	31.813	90.000	73.500	256.031	16.500	6.05
3-12	17	BUMPER	AFFF	60	60.0	28.906	19.688	500.926	243.421	34.250	32.156	91.364	76.250	257.505	15.114	5.54
3-13	20	BUMPER	AFFF	_60	60.1	28.938	19.719	501.852	244.079	34.281	32.000	91.591	75.000	257.773	16.591	6.05
3-14	28	BUMPER	AFFF	60	59.6	39.438	31.219	813.462	569.444	23.875	20.000	17.502	2.425	244.017 72.773	15.077 0.227	5.83 0.3
1-1	H 1-1	HANDLINE	AFFF	<u>60</u> 60	60.1 60.1	14.750 37.563	11.250 35.094	138.158 757.407	65.385 685.577	30.344 30.375	30.313 30.188	62.955	62.727	71.830	1.364	1.86
1-3	H 3-1	HANDLINE	AFFF		60.0	35.094	32.531	685.577	608.333	30.188	30.063	61.818	60.909	77.244	0.909	1.10
1-5	3	HANDLINE	AFFF	60	60.0	17.750	14.813	202.632	139.474	28.531	28.531	49.318	49.318	63.158	0.850	1.30
1-6	4	HANDLINE	AFFF	60	60.1	45.594	43.500	999.074	937.037	28.594	28.594	49.773	49.773	62.037	0.701	1,12
1-7	. 5	HANDLINE	AFFE	<u>.6</u> 0	60.0	43.500	41.469	937.037	875.962	28.594	28.594 24.813	49.773 24.169	<u>49.773</u> 24.169	61.075 64.815	0.701	2.08
1-8	13 20	HANDLINE	AFFF	. <u>60</u> 60	60.0	45.625 17.000	43.438 14.063	186.486	935.185 123.684	24.813 25.094	25.094	26.136	26.136	62.802	1.594	2.47
1-10	- 20	HANDLINE	AFFF	60	60.1	45.563	43.375	998.148	933.333	25.094	25.094	26.136	26.136	64.815	0.691	1.05
1-11	22	HANDLINE	AFFF	60	60.2	43.375	41.344	933.333	872.115	25.093	25.094	26.136	26.136	61.218	1.519	2.42
1-12	28	HANDLINE	AFFF	60	60.0	27.938	25.813	472.222	409.259	26.063	26.062	33.184	33.180	62.963	1.562	2.42
2.1	H 1-3	HANDLINE	AFFF	120	120.1	15.250	8.188	148.684	3.750	35.813	35.188	102.917	98.500	74.934	2.150	2.96
$-\frac{2\cdot 2}{2\cdot 3}$	H 2-3 H 3-3	HANDLINE HANDLINE	AFFF	<u>60</u>	60.2 61.2	13.250 12.969	9.625 9.344	106.579 100.658	32.500 26.875	30.813 26.313	30.500 26.000	66.250 35.000	32.729	74.079 73.783	2.159	2.83 5.38
2.5	1	HANDLINE	AFFF	60	60.0	45.625	43.438	1000.000	935.185	39.719	39.719	129.502	129.502	64.815	2.178	3.25
2-6	2	HANDLINE	AFFF	60	60.1	43.437	41.438	935.185	875.000	39.719	39.719	129.502	129.502	60.185	1.987	3.20
2-7_	8	HANDLINE	AFFF	60	60.1	18.750	15.875	223.684	162.162	36.219	36.219	105.750	105.750	61.522	1.636	2.59
2-8	9	HANDLINE	AFFF	_60	60.0	15.875	13.000	162.162	101.316	36.218	36.218	105.750	105.750	60.846	1.657	2.65
2.9	15/2	HANDLINE	AFFF	60	60.0	18.531 45.531	15.781 43.406	219.079 997.222	160.135 934.259	36.094 30.563	36.094 30.563	104.792 64.545	104.792 64.545	58.944 62.963	1.562 1.732	2.58
2-10	15/3 16/2	HANDLINE	AFFF	. <u>60</u> .	60.1 60.0	15.781	12.906	160.135	99.359	36.094	36.094	104.792	104.792	60.776	1.530	2.46
2-12	16/3	HANDLINE	AFFF		60.1	43.406	41.375	934.259	873.077	30.563	30.563	64.545	64.545	61.182	1.700	2.70
2-13	17	HANDLINE	AFFF	60	60.0	45.531	43.344	997.222	932.407	36.094	36.094	104.792	104.792	64.815	2.029	3.04
3-1	_H 1-6	HANDLINE	AFFF	60	60.2	45.688	43.313	1001.370	931.481	32.063	31.500	75.500	71.000	69.888	4.500	6.05
3-2	H 2-6	HANDLINE	AFFF	60	60.0	43.313	40.938	931.481	859.615	31.500	30.969	71.000	67.292	71.866 74.430	3.708 3.655	4.91
3-3 3-5	H 3-6	HANDLINE HANDLINE	AFFF AFFF	60 60	60.0 60.1	40.938 19.688	<b>38.50</b> 0 16.875	859.615 243.421	785.185 183.784	30.969 32.406	30.438 32.406	67.292 78.250	63.636 78.250	59.637	3.357	5.30 5.30
3-6	3 4/5	HANDLINE	AFFF	60	59.9	45.531	43.406	997.222	934.259	39.594	39.219	128.835	126.834	62.963	5.380	7.87
3.7	1/1	HANDLINE	WATER	60	60.0	45.281	43.219	989.815	928.704	23.813	23.813	17.002	17.002	61.111	3.464	5.36
3-8	?	HANDLINE	AFFF	60	60.1	45.594	43.500	999.074	937.037	39.500	39.313	128.335	127.335	62.037	4.475	5.73
3.9	14	HANDLINE	AFFF	60	60.2	28.875	26.844	500.000	439.815	34.094	34.063	90.227	90.000	50.185	3.468	5.45
3-10	18	HANDLINE	AFFF	60 50	50.1 60.2	19.688	16.750	243.421 244.079	181.081 184.459	32.156 32.000	32.094 31.938	76.250 <sub>~</sub> 75.000	75.750 74.500	52.340 59.619	3.836 3.879	. 5.80 5.11
3-11	21 25	HANDLINE HANDLINE	AFFF AFFF	50 50	60.2 50.0	19 719 45.625	1 <b>6</b> .906 <b>43</b> .469	1000.000	936.111	23.906	23.813	17.752	17.002	63.889	3.079 4.161	ن. ا ا في ا
3-13	26	HANDLINE	AFFF	50	50.0	43.469	41.438	936.111	375.000	23.875	23.875	17.502	17.502	51.111	3.241	5.04
3-14	27	HANDLINE	AFFF	60	50 1	41.438	39.438	375.000	813.462	23.875	23.875	17.502	17.502	61.538 -	3.071	4.75



## AND RESULTS

	1555	TANK		1		CALC.	TARGET	<del></del>	FLOW		T	AFFE NOR	D CYLINDER
INC	CHES	_	LONS	WATER	AFFF	RATIO	RATIO	ERROR	RATE	AMB.	TEST		CHES
START	END	START	END	USED	USED	a <sub>2</sub>	%	%	(GPM)	TEMP	DATE	START	END
30.813	30.344	66.250	62.955	311.842	3.295	1.05	1	0.05	314.6	56	18-Dec-92		<del></del>
29.313	29.031	53.438	52.031	260.256	1.406	0.54	1	-0.46	261.7	65	18-Dec-92		
24.438	23.969	21.668	18.253	306.384	3.415	1.10	1	0.10	309.8	68	18-Dec-92		
25.813	25.406	31.365	28.409	267.495	2.956	1.09		0.09	270.5	80	24-Jun-93	<u></u>	
23.906	23.188	17.752	13.422	270.200	4.330	1.58	· <del>-</del>	0.58	274.5	81	24-Jun-93		
26.688 25.688	26.344 25.219	37.308 30.455	35.192 27.045	270.809 270.273	2.115 3.409	1.25		0.22 0.25	272.9 273.2	82 83	24-Jun-93 24-Jun-93		
24.125	23.500	19.504	14.739	267.385	4.765	1.75	<del></del>	0.75	272.1	83	24-Jun-93		
26.906	26.469	38.654	35.962	266.071	2.692	1.00	<del>-</del> -	0.00	268.8	86	24-Jun-93		
26.469	26.063	35.962	33.184	261.706	2.777	1.05	1	0.05	264.5	86	24-Jun-93		
27.688	26.313	43.464	35.000	319.712	8.464	2.58	3	-0.14	326.5	74	16-Dec-92		
36.1 <u>25</u>	34.875	105.000	96.000	299.584	9.000	2.92	3	-0.03	307.0	69	17-Dec-92		
34.875	33.500	96.000	85.910	311.786	10.090	3.13	3	0.04	320.8	69	17-Dec-92		
35.313	34.344	99.500	92.045	262.451	7.451	2.76	3	-0.08	269.5	85	22-Jun-93	20.012	
39.563 31.813	39.563 30.813	128.669 73.500	128.669 66.250	256.481	7.751 7.250	2.93	3 3	-0.02 -0.11	263.8 270.6	82 85	23-Jun-93 22-Jun-93	22.813	0.016
34.781	33.719	95.250	87.502	263.939	7.748	2.85	3 3	-0.05	271.7	82	20-May-93		
37.219	36.219	112.886	105.750	265.205	7.136	2.62	3	-0.13	271.9	86	22-Jun-93		
9.531	38.531	128.502	122.708	260.714	5.794	2.17	3	-0.28	266.5	83	23-Jun-93		
37.156	36.094	112.500	104.792	266.112	7.710	2.82	3	-0.06	273.8	83	22-Jun-93		
1.594	30.563	71.750	64.545	265.058	7.205	2.65	3	-0.12	272.3	86	23-Jun-93		
0.562	30.562	64.542	64.542	132.898	4.006	2.93	<del>3</del>	-0.02	269.3	86	23-Jun-93	24.750	12.969
3.813 7.375	32.556 36.375	88.184 113.849	80.208 107.000	264.357 265.595	7.976 6.849	2.93	3	-0.02 -0.16	272.3 270.2	82 82	22-Jun-93 22-Jun-93		
4.156	31.525	90.682	72.000	306.131	18.682	5.75	6	-0.04	323.7	72	17-Dec-92		
6.156	21.625	33.866	7.143	294.444	26.724	8.32	6	0.39	320.6	72	17-Dec-92		
0.563	27.875	64.545	44.618	311.111	19.927	6.02	ó	0.00	331.0	72	17-Dec-92		
4.625	32.406	94.091	78.250	256.579	15.841	5.81	6	-0.03	272.0	82	25-Jun-93		
4.438	32.188	92.727	76.500	254.104	16.227	6.00	6	0.00	270.3	_83	25-Jun-93		
4.500	32.156	93.182	76.250	267.788	16.932	5.95		-0.01	284.2	81	19-May-93		
4.344 5.000	32.094 32.563	92.045 97.000	75.750 79.500	255.681 267.398	16.295 17.500	5.99 6.14	6	0.00	272.0 284.4	<u>83</u> 	25-Jun-93 19-May-93		
4.688	32.219	94.545	76.750	268.421	17.795	6.22		0.04	286.2	80	19-May-93		
4.063	31.813	90.000	73.500	256.031	16.500	6.05	6	0.01	272.5	84	25-Jun-93		
4.250	32.156	91.364	76.250	257.505	15.114	5.54	6	-0.08	272.6	84	25-Jun-93		
4.281	32.000	91.591	75.000	257.773	16.591	6.05	6	0.01	273.9	84	25-Jun-93		
3.875	20.000	17.502	2.425	244.017	15.077	5.82	<u> </u>	-0.03	260.8	87	25-Jun-93		
0.344 0.375	30.313 30.188	62.955 63.182	62.727 61.818	72.773 71.830	0.227 1.364	0.31		-0.69 0.86	72.9 73.1	.56 58	18-Dec-92		
0.188	30.063	61.818	60.909	77.244	0.909	1.16	<u></u>	0.16	78.2	58	18-Dec-92		
8.531	28.531	49.318	49.318	63.158	0.850	1.33	1	0.33	64.0	87	23-Jun-93	30.000	27.500
8.594	28.594	49.773	49.773	62.037	0.701	1.12	1	0.12	62.6	89	23-Jun-93	27.625	25.563
8.594	28.594	49.773	49.773	61.075	1.296	2.08		1.08	62.4	89	23-Jun-93	25.563	21.750
4.813	24.813	24.169	24.169	64.815	0.701	1.07		_0.07	65.5	. 81	24-Jun-93	29.625	27.563 22.938
5.094 5.094	25.094 25.094	26.136 26.136	26.136 26.136	62.802	0.691	1.05		0.05	64.4	83 	24-Jun-93 24-Jun-93	27.625 22.875	20.844
5.093	25.094	26.136	26.136	61.218	1.519	2.42		1.42	62.5	_83	24-Jun-93	20.844	16.375
6.063	26.062	33.184	33.180	62.963	1.562	2.42	<del>- i</del>	1.42	64.5	86	24-Jun-93	16.313	11.719
5.813	35.188	102.917	98.500	144.934	4.417	2.96	3	-0.01	74.6	74	16-Dec-92		
D.813	30.500	66.250	64.091	74.079	2.159	2.83	3	-0.06	76.0	74	16-Dec-92		
6.313	26.000	35.000	32.729	73.783	2.271	5.38	3	0.79	74.6	74	16 Dec-92	05.0:0	
9.719	39.719	129.502	129.502	64.815	2.178	3.25	3	0.08	67.0	82	23-Jun-93	35.063 28.656	28.656 22.813
9.719 6.219	39.719 36.219	129.502 105.750	129.502 105.750	60.185 61.522	1.987	- 3.20 2.59	3	0.07 -0.14	62.1	_82 _86	23-Jun-93 22-Jun-93	35.313	30.500
5.218	36.218	105.750	105.750	60.846	1.657	2.65	3	-0.12	62.5	86	22-Jun-93	30.500	25.625
5.094	36.094	104.792	104.792	58.944	1.562	2.58	3	-0.14	60.5	83	22-Jun-93	34.344	29.750
0.563	30.563	64.545	64.545	62.963	1.732	2.68	3	-0.11	64.6	86	23-Jun-93	34.844	29.750
0.094	36.094	104.792	104.792	60.776	1.530	2.46	3	-0.18	62.3	83	22-Jun-93	29.750	25.250
0.563	30.563	64.545	64.545	61.182	1.700	2.70	3	-0.10	62.8	86	23-Jun-93	29.750	24.750
5.094	36 094 31 500	104.792	104.792	64.815	2.029	3.04	3	0.01	66.8	82	22-Jun-93 18-Dec-92	25.344	19.375
2.063 1.500	30.969	75.500 71.000	71.000 67.292	69.888 71.866	4.500 3.708	6.05 4.91	. <del>6</del>	0.01 -0.18	74.1 75.6	50 50	18-Dec-92		
).969	30.438	67.292	63.636	74.430	3.655	4.68	. 3 .	0.22	78.1	50	18-Dec-92		
2.406	32 406	78.250	78.250	59.637	3.357	5.33	5	0.11	62.9	82	25-Jun-93	35.375	25.500
2.594	39 219	128.835	126.834	<b>62</b> .963	5.380	7.87	0	0.31	68.5	83	25-Jun-93	34.688	24.750
.813	23 513	17.002	17.002	61.111	3.464	5.36	ó	-0.11	64.6		21-May-93	35.063	24.875
.500	39 313	128.335	127.335	62.037	4.475	5.73	3	0.12	66.4	93	25-Jun-93	35.438	25.219
.094	34 063	90.227	90.000	50.185	3.468	5.45	5	-0.09	63.4	84	25-Jun-93	35.531	26.000
.156	32 094 31 938	76.250 <sub>-</sub> 75.000	75.750 74.500	52.340 59.619	3.836 3.879	5.80 5.11	5	-0.03 0.02	66.1 63.3	84 84	25-Jun-93 25-Jun-93	35.250 35.313	25.438 25.375
1.000 1.906	23.313	17.752	17.002	59.819	3.679 4.161	6.11	5 5	0.02	68.1	87	25-Jun-93 25-Jun-93	35.063	25.031
.875	23 375	17.502	17.502	53.007 51.111	3.241	5.04	3	-0.16	64.2	87	25-Jun-93	25.031	15.500
1.875	23 875	17 502	17.502	61.538 -	3.071	4.75	5	-0.21	64.5	87	25-Jun-93	15.500	5.469
	-												



#### APPENDIX A NORDIC MARK IIA EVALUATION MATRIX AND RESULTS

T		7	1	T	PLAN	ACTUAL	Γ		MF	CHANICAL M	ETERED DAT	A
FIGURE				TARGET	DISPENSING	DISPENSING	WATER USAGE - GALS FOAM USAGE - GALS.					
GRAPH	TEST		AGENT	RATIO	TIME	TIME	-		TOTAL			TOTAL
NO.	NO.	TURRET	TANK	%	(sec)	(sec)	START	STOP	USED	START	STOP	USED
1-14	1	ROOF	AFFF	1	60	60.0	28,236	28.733	498	2.380.0	2,385.5	5.4
1-15	2	ROOF	AFFF	1	60	60.1	29.765	30.265	500	2,397.1	2,402.5	5.4
1-16	3	ROOF	AFFF	1	60	60.1	30,265	30.766	501	2.402.5	2.408.2	5.7
1-17	4	ROOF	AFFF	1	60	60.2	30.766	31,279	513	2,408.2	2,413.8	5.6
1-18	5	ROOF	AFFF	1	60	60.2	31,279	31,795	516	2.413.8	2,419.5	5.7
2-16	1	ROOF	AFFF	3	60	60.2	20,742	21.230	488	2,135.4	2,153.4	18.0
2-17	2	ROOF	AFFF	3	60	60.0	22,300	22.802	502	2,174.2	2,190.4	16.2
2-18	3	ROOF	AFFF	3	60	59.9	23,053	23,546	494	2,199.4	2.216.5	17.0
2-19	4	ROOF	AFFF	3	60	60.0	23,546	24,041	495	2,216.5	2.234.1	17.7
2-20	5	ROOF	AFFF	3	60	60.0	24.041	24,536	495	2,234.1	2.251.4	17.3
2-21	1A	ROOF	AFFF	3	60	60.4	18.216 19.740	18.735 20.241	519 501	2.045.8	2,063.6 2,116.5	17.8 17.4
2-22	3A			3	60			<del></del>	476	2,741.6	2.774.1	32.5
3-16 3-17	2	ROOF	AFFF	6	60 60	60.0 60.1	40.369 40.845	40.845	490	2,741.6	2,808.0	33.9
3-17	3	ROOF	AFFF	6	60	60.1	41,335	41,809	474	2.808.0	2,841.9	33.9
3-19	4	ROOF	AFFF	6	60	59.9	41,809	42.283	474	2,841.9	2,875.1	33.2
3-20	5	ROOF	AFFF	6	60	60.1	42.283	42,758	475	2,875.1	2,907.9	32.8
1-14	16	ROOF/BUMP	AFFF	1	60	60.0	28,993	29.765	772	2.388.4	2,397.1	8.7
1-15	17	ROOF/BUMP	AFFF	1	60	60.1	33,131	33.909	778	2,434.5	2,443.1	8.6
1-16	18	ROOF/BUMP	AFFF	1	60	60.1	33,909	34.683	774	2,443.1	2,452.1	9.0
1-17	19	ROOF/BUMP	AFFF	1	60	60.1	34.687	35,442	755	2,452.1	2,461.5	9.4
1-18	20	ROOF/BUMP	AFFF	1	60	60.2	35.442	36.208	766	2,461.6	2,470.4	8.8
2-16	17	ROOF/BUMP	AFFF	3	60	60.0	25.294	26.037	743	2,279.1	2,305.3	26.2
2-17	18	ROOF/BUMP	AFFF	3	60	59.9	26.037	26.757	720	2,305.3	2,329.8	24.5
2-18	19	ROOF/BUMP	AFFF	3	60	60.0	26.757	27.495	738	2,329.8	2,354.7	24.9
2-19	20	ROOF/BUMP	AFFF	3	60 60	60.2	27,495 18,984	28,236 19,740	741 756	2,354.7 2,072.8	2,380.0 2,099.1	25.3 26.3
2-20	2A	ROOF/BUMP		3		60.0				2,498.7	2.550.3	51.6
3-15 3-16	16 17	ROOF/BUMP	AFFF AFFF	6	60 60	60.0 59.9	36,724 37,462	37.462 38.179	738 717	2,496.7	2,550.5	48.2
3-10	18	ROOF/BUMP	AFFF	6	60	60.0	38,179	38,912	733	2,598.5	2.645.7	47.2
3-18	19	ROOF/BUMP	AFFF	6	60	60.1	38,912	39,643	731	2,645.7	2,693.5	47.8
3-19	20	ROOF/BUMP	AFFF	6	60	60.1	39,643	40,369	726	2,693.5	2,741.6	48.1
1-13	6	BUMPER	AFFF	1	60	60.1	28.733	28.993	260	2.385.5	2,388.4	3.0
1-14	7	BUMPER	AFFF	1	60	60.2	31,798	32,071	273	2,419.5	2,422.6	3.1
1-15	8	BUMPER	AFFF	1	60	60.1	32,071	32,333	262	2,422.6	2.425.6	3.0
1-16	9	BUMPER	AFFF	1	60	60.0	32,333	32,596	263	2,425.6	2,428.6	3.0
1-17	10	BUMPER	AFFF	1	60	60.1	32,596	32,863	267	2.428.6	2,431.6	3.0
2-17	7	BUMPER	AFFF	3	60	60.0	22,802	23.053	251	2,190.4	2,199.4 2,260.5	9.0
2-18 2-19	<u>8</u>	BUMPER BUMPER	AFFF	3	60 60	60.1 60.0	24.536 24,791	24.791 25.042	255 251	2,251.5 2,260.5	2,269.7	9.2
2-19	10	BUMPER	AFFF	3	60	60.0	25,042	25,294	253	2,260.5	2,279.1	9.4
2-21	4	BUMPER	AFFF	3	60	59.9	20,241	20,487	246	2.116.5	2,125.0	8.5
2-22	5	SUMPER	AFFF	3	60	60.1	18.735	18,984	249	2.063.6	2.072.8	9.2
3-16	6	BUMPER	AFFF	6	60	60.0	42,758	43.000	242	2,907.9	2,926.4	18.5
3-17	7	BUMPER	AFFF	6	60	59.9	43.000	43,238	238	2.926.4	2,944.1	17.8
3-18	8	BUMPER	AFFF	6	60	59.9	43.238	43,476	238	2,944.1	2,962.8	18.7
3-19	9	BUMPER	AFFF_	6	60	59.9	43.476	43.720	244	2.962.8	2.981.4	18.6
3-20	10	BUMPER	AFFF	6	60	60.0	43.720	43,958	238	2.981.4	3,000.0	18.6
1-14	11	HANDLINE	AFFF	1	60	60.1	32.863	33,131	268	2,431.6	2,434.5	2.9
1-15	12	HANDLINE	AFFF	1	60	60.0	36.208 36.269	36,269 36,332	61 63	2,470.4 2,471.6	2,471.6 2,473.1	1.2
1-16	13	HANDLINE HANDLINE	AFFF AFFF	1	60 60	60.1 60.0	36.332	36.388	56	2,471.6	2,473.1	1.4
1-18	15	HANDLINE	AFFF	1	60	59.9	36.388	36,442	54	2.474.5	2,475.8	1.3
2-15	11	HANDLINE	AFFF	3	60	59.8	21,230	21.290	60	2.153.4	2,155.6	2.2
2-16	12	HANDLINE	AFFF	3	60	60.2	21,290	21,346	57	2,155.6	2,158.1	2.5
2-17	13	HANDLINE	AFFF	3	60	60.1	21.346	21,402	56	2,158.1	2,160.3	2.2
2-18	14	HANDLINE	AFFF	3	60	61.0	21,402	21,461	59	2,160.3	2,162.5	2.2
2-19	15	HANDLINE	AFFF	3	60	59.6	21,461	21.518	57	2,162.5	2.164.7	2.2
3-16	11	HANDLINE	AFFF	6	60	60.0	36.442	36.503	61	2.475.8	2,481.0	5.2
3-17	12	HANDLINE	AFFF	6	60	60.0	36,503	36.555	52	2.481.0	2.485.4	4.4
3-18	13	HANDLINE	AFFF	6	60	60.1	36.555	36.613	58	2.485.4	2,489.7	4.3
3-19	14	HANDLINE	AFFF	ô	60	60.1	36.613	36.670	57	2.489.7	2,494.1	4.4
3-20	15	HANDLINE	AFFF	ŝ	60	59.8	36.670	36.724	54	2.494.1	2,498.7	4.6

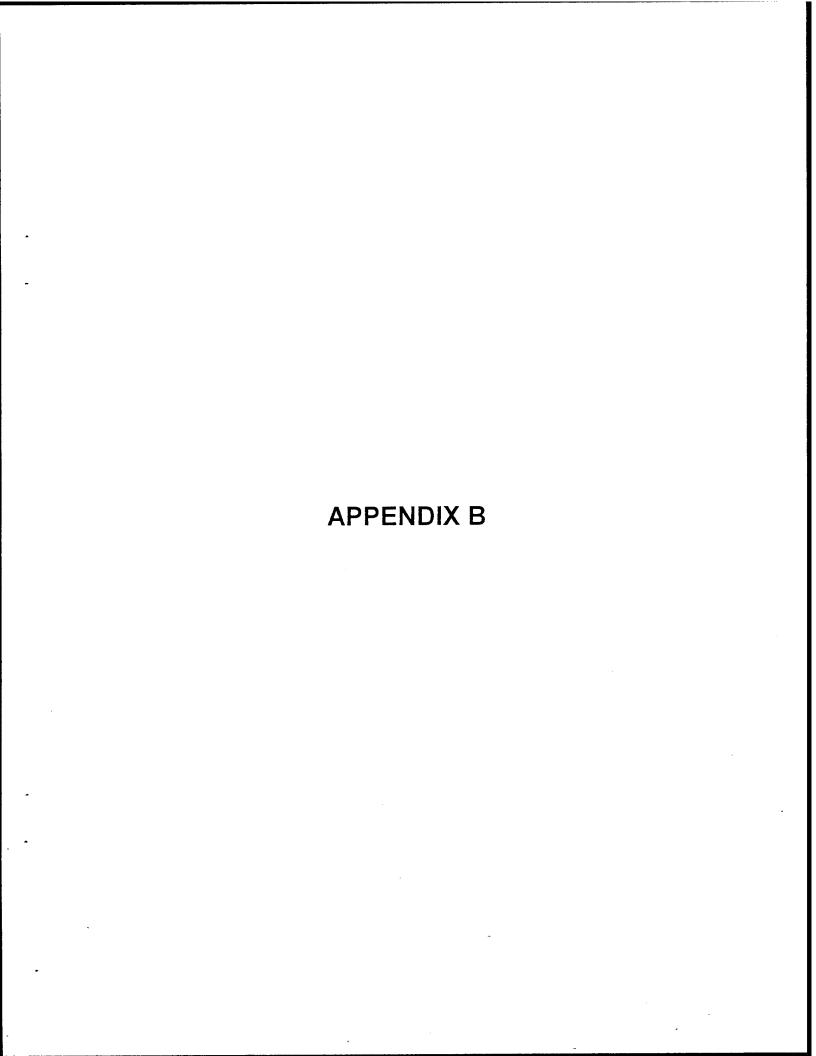


## MATRIX AND RESULTS

## MAGNETIC FLOW METER DATA

FOAM USAGE - GALS. CALC SOLUTION USAGE - GALS FOAM USAGE - GALS. CALC							ELECTRONIC METERED DATA								
No.   Start   Store   USEA   Start   STOP   USEA   Start   STOP   USEA   Start   STOP   USEA   Start   Store   USEA   Start   Start   USEA	MEC				2412		COLUI	TON USAGE					CALC		
No.   START   STOP   USED   N.   START   STOP   USED   START   STOP   USED   N.		FOAI	M USAGE - G				SOLUI	ION OSAGE		100	W OOAGE - C			ERROR	
D         SIANI   300°         SOLO   3585   54   100°         COLOR   571580   375808   3500   5167   6177   6182   598   107   007		OT LOT	0700	-			START	STOP	-	START	STOP		1 1		
2,000   2,000   3,4	-D	START	STOP									5.20	1.07	0.07	
3 2,997   2,406.2 3.7   11.0   0.72   58.07.3   59.77.5   51.95   51.95   5.49   1.08   0.07.2   0.07.	8														
2,402   2,403   5,60   1,02   0.09   0.007.0	0														
3 2 4092 2 24198 5 5 1.08 0.00 90.00 1 0.00	1														
8 2.115. 2.115. 2.115. 4 1.00														-	
8 2198-4 2198-4 162 3198-0 599 3399 5175 5181 55960 51868 3280 228 228 2199-4 22955 1770 319-5 319-5 5187-5 599-6 5000-2 161-6 4 324 0.28 2199-6 22955 1770 319-6 319-5 5187-5 599-7 599-9 5000-2 161-6 4 324 0.28 2199-6 1777 31-6 319-6	6													0.29	
2 2174 2 2193 162 2195 177 334 0.14 2295 2295 2095 2095 2095 2095 2095 2095	8														
4 2 1984	2														
5 2216.5 2294. 17.7 3.34.6 0.44 5293.0 521. 34.4 0.44 5293.0 592 6.022.7 6.002	4														
5 2294   2291   77.3   3.38   0.59   52.500.9   3.455   5.831.0   5.986   19.93   347   0.47   17.0															
9															
1												<del></del>	3.31	0.31	
6 2,7415 2,741 3,225 6.89 0.99 69,712 189,000 177 6.5510 6.5536 32.69 6.39 0.39 0.39 4 2,2860 2,28619 335 6.67 0.67 70,3834 70,000 3188 6.5519 6.553 6.5536 32.69 20,29 14 2,28619 2,28619 335 6.67 0.67 70,3834 70,000 3188 6.5519 6.553 2,200 22 1.021 18,28719 32.6 6.56 0.55 70,3854 70,000 3188 6.5519 6.5519 32.00 52 20 6.21 0.21 18,28719 32.6 6.46 0.46 71,695 71,114 0.15 6.15 6.16 6.67 6.66 71,695 71,114 0.15 6.15 6.27 6.15 71,114 0.15 6.15 6.27 6.15 71,114 0.15 71,114 0.15 6.15 71,114 0.15 6.15 71,114 0.15 6.15 71,114 0.15 71,114 0.15 6.15 71,114 0.15 6.15 71,114 0.15 6.15 71,114 0.15 6.15 71,114 0.15 6.15 71,114 0.15 6.15 71,114 0.15 6.15 71,114 0.15 6.15 71,114 0.15 6.15 71,114 0.15 6.15 71,114 0.15 6.15 71,114 0.15 6.15 71,114 0.15 6.15 71,114 0.15 6.15 71,114 0.15 6.15 71,114 0.15 6.15 71,114 0.15 6.15 71,114 0.15 6.15 71,114 0.15 71,114 0.15 71,114 0.15 71,114 0.15 71,114 0.15 71,114 0.15 71,114 0.15 71,114 0.15 71,114 0.15 71,114 0.15 71,114 0.15 71,114 0.														0.30	
0 2.7741															
4	-														
4 2.8419 2.971 3.32 8 6.46 0.46 77.696 77.996 77.9164 5115 6.6427 6.680.3 31.76 6.18 0.18 2 2.938.4 2.2971 8.7 1.11 0.11 57.910.3 58.671.5 767.4 6.175.3 6.186.2 8.43 1.10 0.10 0.10 0.10 0.10 0.10 0.10 0.1						<del></del>								-0.05	
\$ 2,875.1 2,807.9 32.8 5.46															
2 2.384.4													<del></del>	0.10	
8 2.434.5												<del></del>	<del></del>		
4 2.443.1 2.445.1 9.0 1.15 0.15 06.727.3 03.94.94.1 77.0 6.229.3 0.2299.3 0.2299.3 0.2299.3 0.2299.3 0.2299.3 0.2299.3 0.2299.3 0.2299.3 0.2299.3 0.22	_														
5 2.492.1 2.491.5 9.4 1.23 0.23 8.503.2 776.5 0.248.3 6.285.3 8.36 1.08 0.02 0.23 0.23 0.23 0.23 0.23 0.23 0.23	-					<del></del>									
3 2.2791   2.305.3   2.302.8   2.45   3.29   0.29   54.878.9   55.633.2   760.4   6.092.8   6.117.1   24.40   3.21   0.21   3 2.229.8   2.354.7   2.380.0   2.53   3.30   0.30   56.390.8   67.756.9   77.22   6.141.4   6.165.8   24.53   3.18   0.18   6 2.077.2   2.099.1   2.63   3.33   0.30   0.30   56.390.8   67.756.9   77.22   6.141.4   6.165.8   24.53   3.18   0.18   6 2.077.2   2.099.1   2.63   3.33   0.30   6.364.0   4.793.9   48.495.3   763.5   5.893.2   5.894.1   24.49   3.26   0.26   8 2.498.7   2.550.3   51.6   6.53   0.53   65.540.2   66.311.1   77.70   6.285.0   6.332.7   47.91   6.17   0.17   7 2.550.3   2.598.5   48.2   6.30   0.30   66.3111   67.072.2   67.835.9   789.8   6.379.3   6.425.5   46.32   6.02   0.02   3 2.598.5   2.585.7   47.2   6.05   0.05   67.072.2   67.835.9   789.8   6.379.3   6.425.5   46.32   6.02   0.02   1 2.645.7   2.689.5   47.8   6.14   0.14   67.835.9   68.604   767.7   6.332.9   6.425.1   46.68   6.08   0.08   2 2.885.5   2.388.4   3.0   1.12   0.12   57.653.8   57.910.2   262.6   6.172.2   6.175.1   3.09   1.18   0.18   3 2.419.5   2.422.6   2.426.6   3.0   1.13   0.13   60.937.1   61.195.2   242.2   6.205.6   3.00   1.15   0.15   60.937.1   61.195.2   242.2   6.245.6   3.0   1.11   0.11   61.149.5   61.44													<del></del>		
3 2.2791 2.395.3 26.2 3.41 0.41 95.116.9 95.076.9 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10													3.24	0.24	
8 2.309.8 2.354.7 249 3.26 0.29 55.833.2 56.390.8 767.3 6,117.4 6,141.2 23.96 3.12 0.12 1.2.364.7 2.380.0 25.3 3.30 0.50 56.390.8 767.3 6,117.4 6,141.2 23.96 3.12 0.12 1.2.364.7 2.380.0 25.3 3.30 0.50 56.390.8 767.3 7.2.5 6,141.4 6,165.8 24.53 3.18 0.18 6.2.072.8 2.099.1 26.3 3.36 0.36 47.737.9 48,485.3 763.5 5.893.3 5.884.1 24.99 3.26 0.26 8.2.498.7 2.550.3 516 6.53 0.53 65.540.2 66.311.1 777.0 6.285.0 6.332.7 47.91 6,17 0.17 7.2.526.0 7.2.2.50.3 51.6 6.53 0.53 65.540.2 66.311.1 777.0 6.285.0 6.332.7 47.91 6,17 0.17 7.2.526.0 7.2.2.50.3 51.6 6.53 0.53 65.540.2 66.311.1 777.0 6.285.0 6.332.7 47.91 6,17 0.17 7.2.526.0 7.2.2.50.3 51.6 6.53 0.53 65.540.2 66.311.1 777.0 6.285.0 6.332.7 47.91 6,17 0.17 7.2.526.0 7.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2															
8 2.498.7	-												<del></del>		
1													3.18	0.18	
8 2.498.7 2.559.3 516 6.53 0.53 65.540.2 66.311.1 777.0 6.285.0 6.332.7 47.91 6.17 0.17 7.2559.3 2.598.5 48.2 6.30 0.30 6.6311.1 67.072.2 757.1 6.332.9 5.378.1 48.35 5.91 0.09 3.2 5.598.5 2.645.7 47.2 6.05 0.05 67.072.2 67.835.9 769.8 6.379.3 6.425.5 46.32 6.02 0.02 1.2 6.645.7 2.693.5 2.645.7 47.2 6.05 0.05 67.072.2 67.835.9 769.8 6.379.3 6.425.5 46.32 6.02 0.02 1.2 6.645.7 2.693.5 2.741.6 46.1 6.21 0.21 68.604.6 99.371.2 772.7 6.472.1 6.518.7 46.73 6.05 0.08 0.08 0.2 385.5 2.384.8 3.0 1.12 0.12 57.653.8 57.910.2 22.6 6.172.2 6.175.1 3.09 1.18 0.18 0.18 0.2 385.5 2.384.8 3.0 1.12 0.12 57.653.8 57.910.2 22.6 6.172.2 6.175.1 3.09 1.18 0.18 0.18 0.2 385.5 2.384.8 3.0 1.12 0.12 60.680.5 60.937.1 262.7 6.206.4 6.209.5 3.16 1.20 0.20 0.20 0.2 422.6 2.422.6 3.1 1.12 0.12 60.680.5 60.937.1 61.195.2 264.2 6.209.6 6.212.5 3.12 1.18 0.18 0.18 0.2 422.6 2.422.6 3.0 1.13 0.13 60.391.7 61.195.2 264.2 6.209.6 6.212.5 3.12 1.18 0.18 0.18 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19	-											<del></del>	3.26	0.26	
8         2.4867         2.550.3         2.598.5         48.2         6.30         0.30         66.311.1         67.072.2         787.1         6.332.9         6.378.1         45.35         5.91         9.09           3         2.598.5         2.645.7         47.2         6.05         0.05         67.072.2         67.835.9         68.046.4         767.3         6.425.5         6.472.1         48.68         6.00         0.02           6         2.693.5         2.741.6         48.1         6.21         0.21         68.604.6         69.371.2         772.7         6.472.1         6.518.7         46.73         6.05         0.05           6         2.693.5         2.741.6         48.1         6.21         0.21         0.21         68.604.6         69.371.2         772.7         6.472.1         6.518.7         46.73         6.05         0.05           3         2.4226.6         3.1         1.12         0.12         57.658.8         57.910.2         262.6         6.272.5         3.12         1.18         0.18           3         2.4226.6         2.4256.8         3.0         1.11         0.11         61.1952.2         264.2         6.209.6         6.212.5         3.12         1.18	-									6.285.0	6.332.7	47.91	6.17	0.17	
3 2.598.5 2.694.7 47.2 6.05 0.05 67.072.2 67.835.9 769.8 6.379.3 6.425.5 48.32 6.02 0.02 1 2.645.7 2.683.5 47.8 6.14 0.14 67.835.9 68.604.6 77.73 6.425.5 6.472.1 46.68 6.08 0.08 6 2.693.5 2.741.6 48.1 6.21 0.21 68.604.6 69.371.2 772.7 6.472.1 6.518.7 46.73 6.05 0.05 0.05 0.2 385.5 2.741.6 48.1 6.21 0.21 68.604.6 69.371.2 772.7 6.472.1 6.518.7 46.73 6.05 0.05 0.05 0.2 385.5 2.741.6 48.1 0.21 0.12 0.12 67.633.8 67.910.2 262.6 6.172.2 6.175.1 3.09 1.18 0.18 0.18 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19						<del></del>							5.91	-0.09	
\$\begin{array}{c c c c c c c c c c c c c c c c c c c	$\longrightarrow$											46.32	6.02	0.02	
1.   1.   1.   1.   1.   1.   1.   1.											6,472.1	46.68	6.08	0.08	
0 2.985.5 2.988.4 3.0 1.12 0.12 57.653.8 57.910.2 262.6 6.172.2 6.175.1 3.09 1.18 0.18 3.2 4.19.5 2.422.6 3.1 1.12 0.12 60.880.5 60.937.1 262.7 6.206.4 6.209.5 3.16 1.20 0.20 0.20 0.20 0.20 0.20 0.20 0.20											6,518.7	46.73	6.05	0.05	
3 2,419.5 2,422.6 3.1 1.12 0.12 60.680.5 60.937.1 262.7 6,206.4 6,209.5 3.16 1.20 0.20 2 2,422.6 2,425.6 3.0 1.13 0.13 60.937.1 61.195.2 61.49.5 264.2 6.209.6 6.212.5 3.12 1.18 0.18 3 2,425.6 2,428.6 3.0 1.11 0.11 61.195.2 61.449.5 260.4 6,212.7 6.215.5 3.00 1.15 0.15 7 2,428.6 2,431.6 3.0 1.11 0.11 61.449.5 61.705.4 261.9 6,215.7 6.218.6 3.05 1.16 0.16 1.2190.4 2,199.4 90 3.47 0.47 51.579.0 51.834.3 261.4 5.980.7 5.989.7 9.14 3.50 0.50 1.16 0.16 1.22.251.5 2,260.5 9.0 3.41 0.41 63.343.0 33.40.0 35.360.1 3264.4 6.040.5 6.049.6 9.29 3.51 0.51 1.22.251.5 2,260.5 9.0 3.41 0.41 63.343.0 53.340.0 53.360.1 3 264.4 6.040.5 6.049.6 9.29 3.51 0.51 1.22.251.5 2,260.5 9.0 3.41 0.41 63.343.0 53.340.0 53.264.4 6.040.5 6.049.6 9.29 3.51 0.51 1.22.251.5 2,260.5 9.0 3.41 0.41 63.490.7 9.49.264.5 6.049.8 6.068.7 9.06 3.44 0.44 3.2 2.269.7 2,279.1 9.4 3.59 0.59 53.858.7 34.116.9 264.4 6.058.8 6.067.7 9.01 3.41 0.41 62.115.5 2.1250 8.5 3.34 0.34 49.07.9 9.264.5 5.20.1 8.5 3.34 0.34 49.07.9 9.264.5 5.20.1 8.5 3.34 0.34 49.07.9 9.264.5 5.20.1 8.5 3.34 0.34 49.07.9 9.264.5 5.20.1 8.5 3.34 0.34 49.07.9 9.264.5 5.20.1 8.5 3.34 0.34 49.07.9 9.264.5 5.20.1 8.5 3.34 0.34 49.07.9 9.264.5 5.20.1 8.5 3.34 5.35 0.53 0.53 0.53 0.20.1 8.20.									262.6	6,172.2	6,175.1	3.09	1.18	0.18	
2 2.422.6 2.425.6 3.0 1.13 0.13 60.937.1 61.195.2 264.2 6.209.6 6.212.5 3.12 1.18 0.18 3 2.425.6 2.428.6 3.0 1.11 0.11 61.195.2 61.449.5 260.4 6.212.7 6.215.5 3.00 1.15 0.15 7 2.428.6 2.431.6 3.0 1.11 0.11 61.195.2 61.449.5 261.9 6.215.7 6.218.6 3.05 1.16 0.16 11 2.190.4 2.199.4 9.0 3.47 0.47 51.579.0 51.834.3 261.4 5.980.7 5.989.7 9.14 3.50 0.50 12 2.251.5 2.260.5 9.0 3.41 0.41 53.343.0 53.601.3 264.4 6.040.5 6.049.6 9.29 3.51 0.51 12 2.250.5 2.259.7 9.2 3.54 0.54 53.601.3 53.851.3 263.4 6.049.8 6.058.7 9.06 3.44 0.44 33 2.259.7 2.279.1 9.4 3.59 0.59 53.858.7 54.116.9 264.4 6.058.8 6.067.7 9.01 3.41 0.41 6 2.116.5 2.125.0 8.5 3.34 0.34 49.007.9 49.264.5 262.7 5.901.4 5.910.1 8.85 3.37 0.37 9 2.053.6 2.072.8 9.2 3.56 0.56 47.483.8 47.737.9 260.2 5.850.2 5.859.2 9.18 3.53 0.53 2 2.907.9 2.926.4 18.5 7.08 1.08 71.916.4 72.170.4 254.5 6.681.3 6.699.3 17.94 7.05 1.05 8 2.926.4 2.944.1 17.8 6.94 0.94 72.170.9 72.427.6 262.8 6.699.5 6.717.1 17.80 6.77 0.77 8 2.944.1 2.926.8 18.7 7.28 1.28 72.247.7 72.268.0 264.4 6.735.1 6.753.1 18.18 6.88 0.88 8 2.981.4 38.6 7.08 1.08 72.894.1 72.894.1 72.803.0 63.2 6.254.6 6.259.3 1.45 1.25 1.25 1.25 1.25 1.25 1.25 1.25 1.2						<del></del>				6,206.4	6,209.5	3.16	1.20	0.20	
3 2.425.6 2.428.6 3.0 1.11 0.11 61.195.2 61.49.5 260.4 6.212.7 6.215.5 3.00 1.15 0.15 7 2.428.6 2.431.6 3.0 1.11 0.11 61.495.5 61.705.4 261.9 6.215.7 6.218.6 3.05 1.16 0.16 7 2.428.6 2.431.6 3.0 1.11 0.11 61.449.5 61.705.4 261.9 6.215.7 6.218.6 3.05 1.16 0.16 1 2.190.4 2.199.4 9.0 3.47 0.47 51.579.0 51.834.3 261.4 5.980.7 5.989.7 9.14 3.50 0.50 5 2.251.5 2.260.5 9.0 3.41 0.41 53.343.0 53.601.3 264.4 6.040.5 6.049.6 9.29 3.51 0.51 1 2.260.5 2.269.7 9.2 3.54 0.54 53.601.3 53.855.7 263.4 6.049.8 6.058.7 9.06 3.44 0.44 3 2.269.7 2.279.1 9.4 3.59 0.59 53.958.7 54.118.9 264.4 6.058.8 6.067.7 9.01 3.41 0.41 6 2.116.5 2.125.0 8.5 3.34 0.34 49.007.9 49.264.5 262.7 5.901.4 5.910.1 8.85 3.37 0.37 9 2.063.6 2.072.8 9.2 3.56 0.56 47.483.8 47.737.9 260.2 5.850.2 5.859.2 9.18 3.53 0.53 2 2.290.7 9 2.926.4 18.5 7.08 1.08 71.916.4 72.170.4 254.5 6.6881.3 6.699.3 17.94 7.05 1.05 8 2.926.4 2.944.1 17.8 6.94 0.94 72.170.9 72.427.6 262.8 6.699.5 6.717.1 17.80 6.77 0.77 8 2.944.1 2.962.8 18.7 7.28 1.28 72.427.7 72.686.0 264.4 6.775.1 17.80 6.77 0.77 8 2.944.1 2.962.8 18.7 7.28 1.28 72.427.7 72.686.0 264.4 6.715.1 17.80 6.77 0.77 8 2.944.1 2.962.8 18.7 7.28 1.28 72.427.7 72.686.0 264.4 6.715.1 17.80 6.77 0.77 8 2.944.1 2.962.8 1.87 7.28 1.28 72.427.7 72.686.0 264.4 6.715.1 17.80 6.77 0.77 8 2.944.1 2.962.8 1.87 7.28 1.28 72.841.7 3203.7 265.7 6.753.4 6.771.3 18.01 6.78 0.78 8 2.941.4 3.000.0 18.6 7.25 1.25 72.944.1 73.203.7 265.7 6.753.4 6.771.3 18.01 6.78 0.78 8 2.431.6 2.434.5 2.9 1.09 0.09 61.705.4 61.959.4 260.1 6.218.7 6.221.5 2.97 1.14 0.14 1 2.470.4 2.471.6 1.2 1.93 0.93 65.034.2 65.091.3 63.2 6.256.6 6.257.9 1.45 2.29 1.29 1 2.471.6 2.473.1 1.5 2.33 1.33 65.091.3 50.084.3 50.193.7 61.5 5.942.5 1.45 2.29 1.29 1 2.473.1 2.474.5 1.4 2.44 1.44 65.149.0 65.203.1 60.3 6.259.6 6.260.9 1.45 2.27 1.27 5 2.473.1 2.474.5 1.4 2.44 1.44 65.149.0 65.203.1 60.3 6.259.6 6.259.3 1.45 2.29 1.29 1 2.153.4 2.155.6 2.2 3.59 0.59 0.59 50.195.3 50.084.3 50.199.7 61.5 5.942.5 1.50 2.44 0.956 5 2.158.1 2.160.3 2.2 3.78 0.78 50.084.3 50.199.7 61.5 5.9									264.2	6.209.6	6,212.5	3.12	1.18	0.18	
7 2.428.6 2.431.6 3.0 1.11 0.11 61.449.5 61.705.4 261.9 62.15.7 6.218.6 3.05 1.16 0.15 1 2.190.4 2.199.4 9.0 3.47 0.47 51.579.0 51.834.3 261.4 5.980.7 5.989.7 9.14 3.50 0.50 5 2.251.5 2.260.5 9.0 3.41 0.41 53.343.0 35.601.3 264.4 6.040.5 6.049.6 9.29 3.51 0.51 1 2.260.5 2.269.7 9.2 3.54 0.54 53.601.3 53.601.3 264.4 6.040.5 6.049.6 9.29 3.51 0.51 1 2.260.5 2.269.7 9.2 3.54 0.54 53.601.3 53.858.7 263.4 6.049.8 6.058.7 9.06 3.44 0.44 3 2.269.7 2.279.1 9.4 3.59 0.59 53.858.7 54.116.9 264.4 6.058.8 6.067.7 9.01 3.41 0.41 6 2.116.5 2.125.0 8.5 3.34 0.34 49.007.9 49.264.5 262.7 5.901.4 5.910.1 8.65 3.37 0.37 9 2.063.6 2.072.8 9.2 3.56 0.56 47.483.8 47.737.9 260.2 5.850.2 5.859.2 9.18 3.53 0.53 2 2.907.9 2.926.4 18.5 7.08 1.08 71.916.4 72.170.4 254.5 6.881.3 6.699.3 17.94 7.05 1.05 8 2.944.1 2.944.1 17.8 6.94 0.94 72.170.9 72.427.6 262.8 6.699.5 6.717.1 17.80 6.77 0.77 8 2.944.1 2.962.8 18.7 7.28 1.28 72.427.7 72.686.0 72.944.1 264.2 6.735.1 18.18 6.88 0.88 8 2.981.4 3.000.0 18.6 7.25 1.25 72.944.1 73.203.7 265.7 6.753.4 6.771.3 18.10 6.78 8 2.431.6 2.434.5 2.9 1.09 0.09 61.705.4 61.959.4 260.1 6.218.7 6.251.5 2.97 1.14 0.14 2.470.4 2.471.6 1.2 1.93 0.93 65.034.2 65.091.3 63.2 6.256.6 6.257.9 1.45 2.29 1.29 3 2.470.6 2.473.1 1.5 2.33 1.33 65.091.3 65.190.0 63.8 6.256.0 6.259.3 1.45 2.29 1.29 3 2.471.6 2.473.1 1.5 2.33 1.33 65.091.3 65.149.0 63.8 6.256.0 6.259.3 1.45 2.29 1.29 3 2.471.6 2.473.1 1.5 2.33 1.33 65.091.3 65.149.0 63.8 6.256.0 6.259.3 1.45 2.29 1.29 3 2.471.6 2.473.1 1.5 2.33 1.33 65.091.3 50.084.3 59.1 5.938.6 5.940.9 2.43 4.12 1.12 2.474.5 2.475.8 1.3 2.35 1.35 65.203.1 60.3 6.256.0 6.256.0 6.259.3 1.45 2.27 1.27 5 2.155.6 2.158.1 2.5 4.24 1.24 50.084.3 50.139.7 61.5 5.946.8 5.940.9 2.43 4.12 1.12 2.155.6 2.158.1 2.5 4.24 1.24 50.084.3 50.139.7 61.5 5.946.8 5.946.9 2.25 3.65 0.65 5 2.158.1 2.160.3 2.2 3.59 0.59 50.195.3 50.249.6 60.6 5.946.3 5.946.9 2.25 3.65 0.65 5 2.158.1 2.160.3 2.2 3.59 0.59 50.195.3 50.249.6 60.6 5.946.3 5.948.9 2.25 3.65 0.65 5 2.158.1 2.160.3 2.2 3.59 0.59 0.59 50.195.3 50.249.6 60.							61,195.2	61,449.5	260.4	6.212.7	6,215.5		-		
1 2.190.4 2.199.4 9.0 3.47 0.47 51.579.0 51.834.3 261.4 5.980.7 5.989.7 9.14 3.50 0.50 5.2251.5 2.260.5 9.0 3.41 0.41 53.343.0 33.8561.3 264.4 6.040.5 6.049.6 9.29 3.51 0.51 0.51 2.260.5 2.269.7 9.2 3.54 0.54 53.601.3 53.8567. 263.4 6.049.8 6.058.7 9.06 3.44 0.44 3.2269.7 2.279.1 9.4 3.59 0.59 53.858.7 54.116.9 264.4 6.058.8 6.067.7 9.01 3.41 0.41 0.41 0.41 0.41 0.41 0.41 0.41 0					1.11	0.11	61,449.5	61,705.4	261.9	6,215.7	6.218.6	3.05	1.16		
5         2,251.5         2,260.5         9,0         3,41         0,41         53,343.0         53,601.3         284.4         6,040.5         6,049.6         9,29         3,51         0,51           1         2,260.5         2,269.7         9,2         3,54         0,54         53,601.3         53,858.7         261.4         6,049.8         6,058.7         9,06         3,44         0,44           3         2,269.7         9,271         9,4         3,59         0,59         53,858.7         54,116.9         264.4         6,058.8         6,067.7         9,01         3,41         0,41           6         2,116.5         2,125.0         8.5         3,34         0,34         49,007.9         49,264.5         262.7         5,901.4         5,910.1         8,85         3,37         0,37           9         2,063.6         2,072.8         9.2         3,56         0,56         47,483.8         47,737.9         260.2         5,850.2         5,859.2         9,18         3,53         0,53           2         2,907.9         2,926.4         18,5         7,08         1,08         7,2170.9         72,427.6         262.8         6,689.5         6,717.1         17.90         7,705 <td< td=""><td>-</td><td>-</td><td></td><td>9.0</td><td>3.47</td><td>0.47</td><td>51,579.0</td><td>51.834.3</td><td>261.4</td><td>5,980.7</td><td>5,989.7</td><td></td><td><del></del></td><td></td></td<>	-	-		9.0	3.47	0.47	51,579.0	51.834.3	261.4	5,980.7	5,989.7		<del></del>		
1 2.260.5 2.269.7 9.2 3.54 0.54 53.601.3 53.858.7 263.4 6.049.8 6.058.7 9.06 3.44 0.44 3.2 269.7 2.279.1 9.4 3.59 0.59 53.858.7 54.116.9 264.4 6.058.8 6.067.7 9.01 3.41 0.41 6.216.5 2.125.0 8.5 3.34 0.34 49.007.9 49.264.5 262.7 5.901.4 5.910.1 8.85 3.37 0.37 0.37 0.37 0.37 0.37 0.37 0.37					3.41	0.41	53,343.0	53.601.3	264.4	6,040.5			<del></del>		
3				9.2	3.54	0.54	53,601.3	53.858.7	263.4						
6         2.116.5         2.125.0         8.5         3.34         0.34         49.007.9         49.264.5         262.7         5.901.4         5.910.1         8.85         3.37         0.37           9         2.063.6         2.072.8         9.2         3.56         0.56         47.483.8         47.737.9         260.2         5.850.2         5.850.2         9.18         3.53         0.53           2         2.907.9         2.926.4         18.5         7.08         1.08         71.916.4         72.170.4         254.5         6.681.3         6.699.3         17.94         7.05         1.05           8         2.926.4         2.944.1         17.8         6.94         0.94         72.170.9         72.427.6         262.8         6.699.5         6.717.1         17.80         6.77         0.77           8         2.944.1         2.962.8         18.7         7.28         1.28         72.427.7         72.686.0         264.4         6.717.1         17.80         6.77         0.77           8         2.941.1         3.000.0         18.6         7.08         1.08         72.944.1         73.203.7         265.7         6.753.4         6.771.3         18.01         6.78         0.78	3			9.4	3.59	0.59	53,858.7								
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2   2.907.9   2.926.4   18.5   7.08   1.08   71.916.4   72.170.9   2.93.3   5.001.0		2.063.6	2.072.8	9.2	3.56	0.56	47.483.8								
8         2.926.4         2.944.1         2.962.8         18.7         7.28         1.28         72.477.7         72.686.0         264.4         6.717.5         6.734.8         17.50         6.62         0.62           4         2.962.8         2.981.4         18.6         7.08         1.08         72.686.0         72.944.1         264.2         6.735.1         6.753.1         18.18         6.88         0.88           8         2.981.4         3.000.0         18.6         7.25         1.25         72.944.1         73.203.7         265.7         6.753.4         6.771.3         18.01         6.78         0.78           8         2.431.6         2.434.5         2.9         1.09         0.09         61.705.4         61.959.4         260.1         6.218.7         6.221.5         2.97         1.14         0.14           1         2.470.4         2.471.6         1.2         1.93         0.93         65.034.2         65.991.3         63.2         6.256.0         6.257.9         1.45         2.29         1.29           3         2.471.6         2.473.1         1.5         2.33         1.33         65.091.3         63.3         6.256.0         6.259.3         1.45         2.27         <	2	2,907.9	2.926.4	18.5	7.08	1.08						<del></del>	+		
8         2,944,1         2,962,8         18,7         7,28         1,28         72,227,7         72,000,0         20,000,0         3,75,1         18,18         6,88         0,88           4         2,981,4         3,000,0         18,6         7,25         1,25         72,944,1         73,203,7         265,7         6,753,4         6,771,3         18,01         6,78         0,78           8         2,981,4         3,000,0         18,6         7,25         1,25         72,944,1         73,203,7         265,7         6,753,4         6,771,3         18,01         6,78         0,78           8         2,431,6         2,434,5         2.9         1,09         0,09         61,705,4         61,959,4         260,1         6,218,7         6,221,5         2,97         1,14         0,14           1         2,470,4         2,471,6         1,2         1,93         0,93         65,031,3         65,091,3         63,2         6,256,6         6,257,9         1,45         2,29         1,29           3         2,471,6         1,2         1,33         65,091,3         65,149,0         63,8         6,258,0         6,259,3         1,45         2,27         1,27           3         2,473,	8	2.926.4	2,944.1	17.8											
4         2,962.8         2,981.4         18.6         7,08         1.06         7,236.0         1,08         7,236.0         1,08         1,25         72,944.1         73,203.7         265.7         6,753.4         6,771.3         18.01         6,78         0,78           8         2,431.6         2,434.5         2.9         1.09         0.09         61,705.4         61,959.4         260.1         6,218.7         6,221.5         2.97         1,14         0,14           1         2,470.4         2,471.6         1.2         1.93         0.93         65,034.2         65,091.3         63.2         6,256.6         6,257.9         1,45         2,29         1,29           3         2,471.6         2,473.1         1.5         2,33         1,33         65,091.3         65,149.0         63.8         6,258.0         6,259.3         1,45         2,27         1,27           5         2,473.1         2,474.5         1,4         2,444         1,44         65,149.0         65,203.1         60.3         6,259.0         1,45         2,41         1,41           4         2,474.5         2,475.8         1,3         2,35         1,35         65,203.1         65,257.0         60.0         6,26	8	2,944.1	2.962.8			<del></del>						<del></del>	<del></del>		
8         2.981.4         3,000.0         18.6         7.25         1.23         72,944.1         73,203.7         25,31.7         5,23.7         1,14         0,14           8         2.431.6         2.434.5         2.9         1.09         0.09         61,705.4         61,959.4         260.1         6,281.7         6,221.5         2.97         1,14         0,14           1         2,470.4         2,471.6         1.2         1.93         0.93         65,034.2         65,091.3         63.2         6,256.6         6,257.9         1,45         2.29         1,29           3         2,471.6         2,473.1         1.5         2,33         1,33         65,091.3         65,149.0         63.8         6,258.0         6,259.3         1,45         2,27         1,27           4         2,474.5         1.4         2,44         1,44         65,149.0         65,203.1         60.3         6,259.6         6,260.9         1,45         2,41         1,41           4         2,474.5         2,474.5         1.3         2,35         1,35         65,203.1         60.2         60.0         6,261.0         6,262.2         1,43         2,39         1,39           2,152.3         2,152.6	4					<del></del>							<del></del>		
8	8	2.981.4	3,000.0					<del></del>							
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6       2,473.1       2,474.5       1.4       2,44       1,44       65,149.0       63,257.0       60.0       6,261.0       6,262.2       1,43       2,39       1,39         4       2,474.5       2,475.8       1.3       2,35       1,35       65,203.1       65,257.0       60.0       6,261.0       6,262.2       1,43       2,39       1,39         9       2,153.4       2,155.6       2,2       3,57       0,57       50,031.3       50,084.3       59.1       5,938.6       5,940.9       2,43       4,12       1,12         7       2,155.6       2,158.1       2,5       4,24       1,24       50,084.3       50,139.7       61.5       5,941.2       5,942.5       1,50       2,44       -0,56         9       2,158.1       2,160.3       2,2       3,78       0,78       50,139.7       50,195.3       61.7       5,943.8       5,945.9       2,25       3,65       0,65         9       2,160.3       2,162.5       2,2       3,59       0,59       50,195.3       50,249.6       60.6       5,946.3       5,948.3       2,16       3,56       0,56         7       2,162.5       2,164.7       2,2       3,72       0,72       50	3														
4       2.474.5       2.475.8       1.3       2.35       1.35       65.203.1       65.237.0       65.257.0       65.203.1       65.257.0       65.203.1       65.203.1       65.203.1       65.203.1       65.203.1       59.203.1       59.203.1       59.243       4.12       1.12         7       2.155.6       2.158.1       2.5       4.24       1.24       50.084.3       50.139.7       61.5       5.940.2       5.940.5       1.50       2.44       -0.56         6       2.158.1       2.160.3       2.2       3.78       0.78       50.139.7       50.195.3       61.7       5.943.8       5.945.9       2.25       3.65       0.65         9       2.160.3       2.162.5       2.2       3.59       0.59       50.195.3       50.249.6       60.6       5.946.3       5.948.3       2.16       3.56       0.56         7       2.162.5       2.164.7       2.2       3.72       0.72       50.249.7       50.302.0       58.4       5.948.6       5.950.8       2.33       3.99       0.99         1       2.475.8       2.481.0       5.2       7.85       1.85       65.257.0       65.331.6       80.7       6.262.3       6.267.2       5.09       6.31 <td><u> </u></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td><del></del></td> <td></td> <td></td> <td></td> <td></td>	<u> </u>									<del></del>					
0     2.153.4     2.155.6     2.2     3.57     0.57     50.034.3     50.084.3     35.1     3.50.084.3     35.1     3.50.084.5     35.1     35.004.5     35.1     35.0     35.1     35.1     35.0     35.1     35.1     35.1     35.0     35.1     35.1     35.1     35.0     35.1     35.1     35.1     35.1     35.0     35.1     35.1     35.1     35.1     35.1     35.1     35.1     35.1     35.1     35.1     35.1     35.1     35.1     35.1     35.1     35.1<	4	2,474.5				<del></del>									
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	1	2.494 1	2,498.7	4.6	7.85	1 1.85	00,400./	05.340.2	, 33.3	0.200.2					





#### APPENDIX B

## FOAM CONTROL SYSTEM OPERATION OVERVIEW

Extracted from Nordic Systems Inc. Mark II Computerized Foam Proportioning System Service Manual for U.S.A.F. P-19

Figure B-1 shows the simplified **foam control** functional diagram. The system objective is to mix foam from the **foam tank** with water from the **water tank** in the correct proportion to form a **solution**. The solution is sprayed onto the fire through the **roof turret**, **bumper turret**, **or handline**.

In the **automatic mode**, the **Foam Control System** continuously adjusts the foam flow to deliver the correct solution concentration. When the **main pump** is started, water flows through the **turret** or other discharge devices. This flow rate is measured by the **solution paddle wheel flow sensor**. The flow computer calculates the foam flow rate required to get the solution to the percentage set on the control panel. Usually this percentage is **3%**, but can be 0%, 1%, 3% or 6%. The computer opens or closes the **motorized metering valve** to adjust the mixture to the correct value.

The **foam flow rate** is measured by the **foam paddle wheel** flow sensor. From this sensor, the **foam control computer** determines the number of gallons of foam per minute flowing. The percentage of foam in the solution is determined by dividing the foam flow rate by the solution flow rate. If the actual percentage foam in the solution is too high, the computer activates the **motorized metering valve** in the "close" direction tending to reduce the foam flow. Conversely, if the actual percentage foam in the solution is too low, then the metering valve motor is activated to "open" the metering valve, increasing the foam flow rate. The duration that the motor is activated is in all cases a fraction of a second, from ten thousandths of a second to one fifth of a second. The exact duration depends on the difference between the actual and desired foam percentage as set on the foam control computer face plate.

The foam control computer monitors the flow sensors about twice a second and immediately adjusts the metering valve accordingly.

Some solution is pumped around the pump through a restriction known as an **eductor**. The eductor generates a low pressure or a suction at one of its ports. Foam is sucked from the foam tank through the eductor into the solution flow and thence back into the pump. This scheme produces foam with a uniform consistency. The process is known as the **"around the pump method"**. This process thoroughly mixes the foam and water into a homogeneous solution. Apart from the fraction that is circulated around the pump, the entire pump output is available for fire fighting by discharge through the roof turret and other discharge devices.

Since foam is drawn into the eductor by a vacuum, the **foam line** is a **low pressure** line with pressures below 10 psi above the metering valve and usually negative below. On the other hand the pump output piping, **the solution line**, is a **high pressure** line with pressures as high as 150 psi.

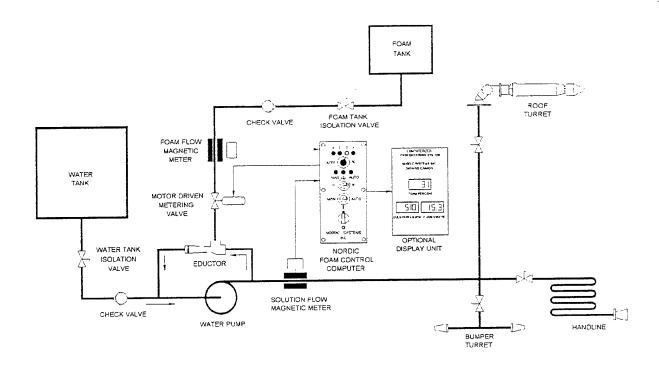


Figure B-1
Simplified foam control system including computer

#### COMPONENTS OF THE FOAM CONTROL SYSTEM

#### 1 Check Valve

There are two **check valves**, one in the foam tank line and one in the water tank line. The check valves allow flow out from a tank but stop flow into a tank. Flow into a tank is an abnormal or fault condition which the check valves prohibit to avoid contamination of the tank contents. The **check valves** work automatically, and are **not controlled by the foam control system**.

#### 2 Foam Valve

The foam valve shown in figure 1 is a pneumatically operated valve. Unless the foam valve is open, no foam can enter into the solution, only pure water will discharge from the turret. The **foam valve** is not controlled in any way by the foam computer. There are no electrical signals from the foam control computer to open or close the foam valve. The foam valve is manually activated by the operator through a three position pneumatic switch on the dashboard.

## 3 Foam Magnetic Flow Meter (originally a paddle wheel)

The foam magnetic flow meter (previously a paddle wheel) senses the flow of foam through the pipe from the foam tank to the eductor. The eductor which is a narrowing in the pipe around the pump, produces a low pressure or suction at the foam inlet port, thus foam is drawn into this eductor port. As the foam flows, the flow meter generates an electrical signal which is sent to the foam control computer, which calculates the actual percentage foam in the solution. Once this calculation is complete, the computer knows whether the mixture is too rich, too lean, or just right. Based upon the calculation, the computer adjusts the foam flow rate to the desired amount by opening or closing the motor driven metering valve. If the flow rate is too slow, the metering valve motor rotates the valve to increase the opening through which foam can flow. If the flow rate is too high, the metering valve is rotated to reduce the opening through which the foam can flow.

#### 4 The Metering Valve

The metering valve is used to ensure that a measured volume flows through it. It consists of a ball valve driven by an electric motor, coupled through a reduction gear. This increases the motor torque or turning power and reduces its speed, both desirable properties in this application.

The motor is driven directly from the vehicles 24 Volt battery. Since it is a DC motor, reversing the polarity reverses the direction in which the motor rotates. Reversing the motor polarity is controlled by the computer to open/close the valve, thus increasing/decreasing respectively the foam percentage in the solution. Despite the gear reduction, the motor spins the metering valve so quickly that the valve can rotate from full off to full on in a couple of seconds. The computer attempts to maintain the foam percentage within one tenth of one percent of the selected value. In order to control the foam percentage in the solution to better than one tenth of a percent, the metering valve motor is pulsed as short as twenty thousandths (20/1000) of a second. For the pulse duration, the full battery voltage is applied to the motor. The average voltage varies widely depending on the duty cycle.

Needless to say, it is crucial that the metering valve and motor drive turn freely without sticking or jamming otherwise these very short duration control pulses will produce no valve correction and the foam control system will loose its "fine touch" or in the worst case, cease to operate at all. The metering valve requires the most attention and service of all the components in the system.

#### 5 Eductor

The eductor produces suction when solution pumped "around the pump" is forced to flow through a restriction or narrowing in the pipe diameter. This low pressure, sometimes loosely called a vacuum, sucks foam concentrate from the foam tank into the eductor where it mixes with the water based solution. The rate at which foam is drawn into the eductor is controlled by the foam control computer. The foam control computer opens or closes the metering valve to maintain the solution foam concentration at the desired value. There are no moving parts in the eductor, it is simply a precisely shaped restriction in the pipe with a duct near the point where the restriction is greatest. The restriction is

shaped like the cross section of an aircraft wing. The restriction forces the fluid to increase in velocity (venturi effect) and in so doing, its pressure must fall, creating suction.

#### 6 Main Pump

The **main pump**, when engaged by the operator, is driven by the vehicle engine. It provides the pumping action for the entire system. The pump consists primarily of an **impeller** which is spun by the vehicle motor to force solution out the discharge ports.

#### 7 Solution Magnetic Flow Meter (originally a paddle wheel flow sensor)

This is similar to the foam flow sensor except that the flow rates are usually a least fifteen times greater. With the roof turret active, the solution flow rate is typically about 500 GPM while the foam flow rate would be 30 GPM for 6% foam solution. The solution magnetic flow meter would normally operate at pressures around 150 PSI, while the foam magnetic flow meter is experiencing a pressure from a foam column no more than six feet high, which creates a head of less than 3 PSI. This is because the foam is **gravity fed** to the foam metering valve and sucked through the metering valve by the eductor vacuum. The foam tank is not pressurized.

#### 8 Main Turret Valve

The **main turret valve** is a pneumatically operated valve which the operator uses to turn on the main turret. When the operator activates a switch on the turret handle, compressed air is applied to the valve where it energizes a piston to fully open the main turret valve. This valve is either full open or shut off, it cannot be used to modulate the solution flow through the turret. The dispersion or shape of the turret discharge is controlled by the operator through a foot switch in the cab, near the accelerator pedal.

The main turret valve is not controlled or monitored by the foam control computer. It is operated independently of the computer by the operator. The foam control computer, in automatic mode, will adjust to the actual flow from zero to maximum flow rate. The computer adjusts the metering valve in response to demand, which may come from any or all the discharge nozzles.

#### 9 Main Turret

The main turret is the **primary discharge device** for the vehicle. It is designed to mix the solution with the correct amount of air to give the solution the consistency to extinguish the fire under attack.

#### 10 Water Tank

The water tank 1000 gallons, which will supply the turret for about two minutes operating at 500 GPM. The water is gravity fed from the water tank to the main pump. The tank is not pressurized.

#### 11 Foam Tank

The foam tank holds the concentrated foam for mixing with water to produce the desired percentage solution. The tank holds about 130 gallons of concentrated foam. At normal operating solution percentage, 3%, there is enough foam in the tank to satisfy four

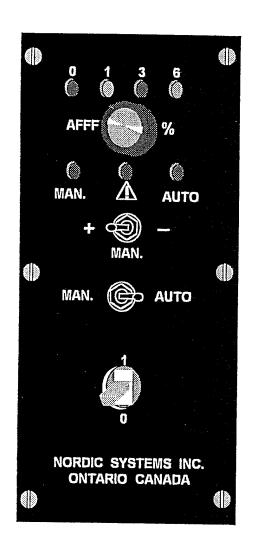
tanks of water, so that the foam tank would only have to be filled every fourth trip to refill the water tank. Like the water tank, the foam tank is not pressurized, its contents flow out under gravity.

### 12 Foam Control Computer

The computer, figure B-2, gets its power from the **truck battery** through a power cable. The computer receives the solution flow rate from the solution flow sensor and the foam flow rate from the foam flow sensor, with this information the foam percentage rate can be calculated. A cable connects computer power to the metering valve providing high currents to open/close the valve. An additional cable provides metering valve position to the computer. Limit switches on the metering valve indicate when it is fully open or fully closed. This limit switch information is critical to the computer which will not attempt to control the foam unless the limit switches are functioning.

The control computer can operate in **manual or automatic mode**. In **manual mode**, the operator activates the metering valve directly. This is done through a spring loaded, center off, momentary contact switch. If the switch is pushed in the "+" direction, the valve rotates in the **open** direction, while a push in the "-" direction rotates the valve in the **close** direction. The longer the switch is held, the greater the valve response. The valve will **remain in the position** it is in when the switch is released (**returns to the center position**). When the limit switches indicate that the valve is fully open/closed, no further motion in the respective direction is permitted. Circuits in the controller **chop the current** applied to the metering valve to slow down the speed of operation thereby making it feasible for the operator to accurately control the valve.

In **automatic mode**, the foam control computer automatically monitors the solution flow. It computes the required foam flow based on the percentage foam setting on the console and the actual solution flow rate. If the actual foam percentage in the solution is too low, it opens the metering valve in proportion to the error. The metering valve motor rotates the valve in a direction to increase the opening through which foam can flow. If the flow rate is too high, the metering valve is rotated in the direction to reduce the opening through which the foam can flow. This monitoring and **adjustment** is carried out about **two times per second**.



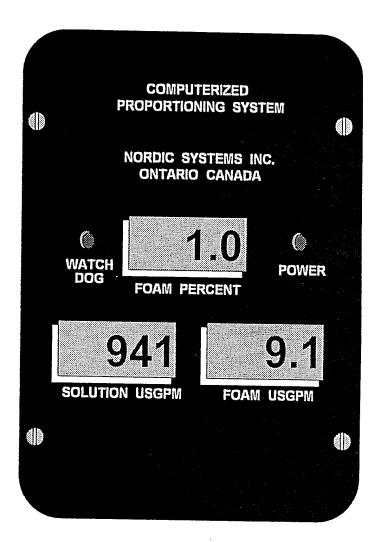


Figure B-2

NORDIC Mark IIA Computerized Foam Proportioning System Dashboard Control and Display Panel



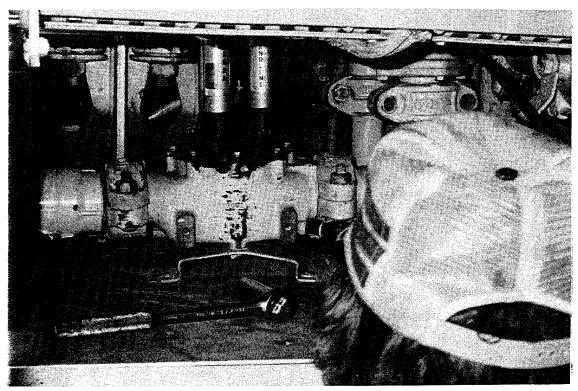


Photo 1 Original Around-the-pump metering System

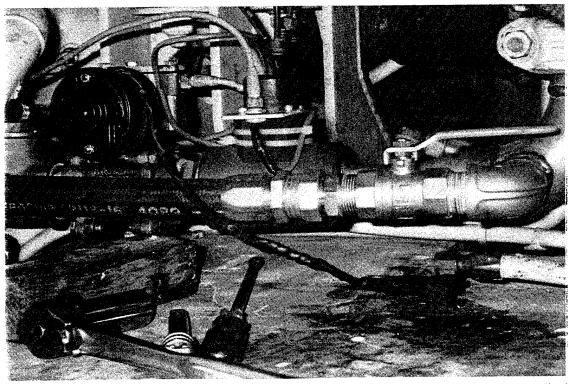
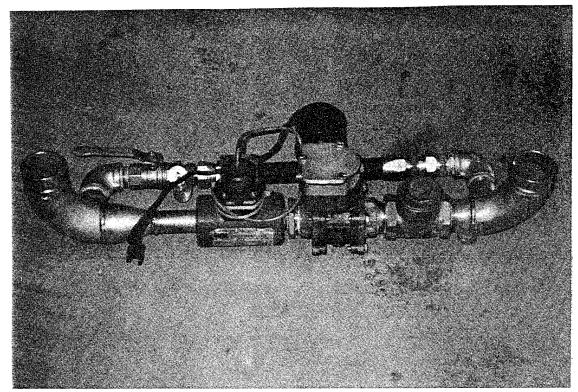


Photo 2 NORDIC Mark IIA Computerized Foam Proportioning System Installed



NORDIC Mark IIA Computerized Foam Proportioning System Valves and Plumbing

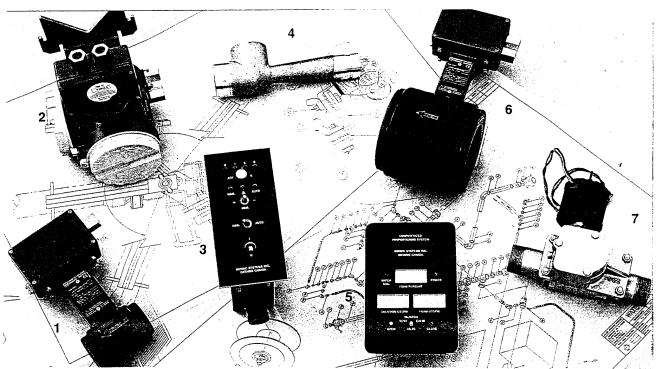
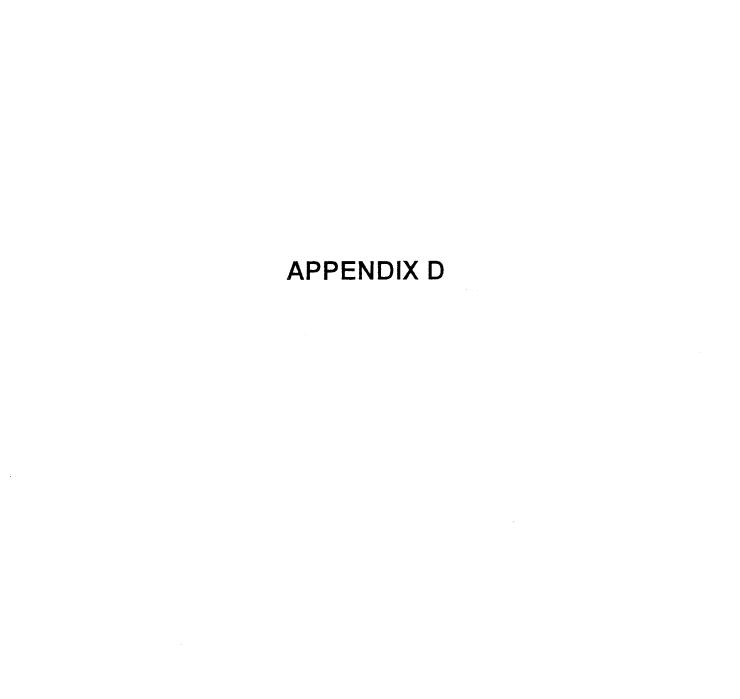


Photo 4 NORDIC system with magnetic flow meters

1. Foam concentrate magnetic flow meter sensor 2. Magnetic flow meter transmitter 3. Computer
4. Eductor 5. Optional digital display 6. Solution magnetic flow sensor 7. metering valve



#### APPENDIX D

MARK IIA AQUEOUS FILM FORMING FOAM
PRECISION METERING SYSTEM
PRODUCT EVALUATION PLAN
JUNE 1992



AIR FORCE CIVIL ENGINEERING SUPPORT AGENCY

TYNDALL AIR FORCE BASE, FLORIDA 32403

D - 1

# MARK IIA AQUEOUS FILM FORMING FOAM PRECISION METERING SYSTEM PRODUCT EVALUATION PLAN JUNE 1992

Revisions to this Evaluation Plan involving changes in scope or resources will be approved by the Chief of Fire Protection, HQ AFCESA.

PREPARED BY:

WADE H. GRIMM, GS-11

Project Manager

REVIEWED BY:

HUGH A. PIKE. GS-12

Project Engineer

RICHARD N. VICKERS, GS-1

Evaluation Manager

24 June 12

APPROVED BY:

PAUL K. LAIRD, GM-14

Chief, Firefighting and Facilities

Branch

CONTRACT SPONSOR: HQ AFCESA/RA

PROJECT SPONSOR: HQ AFCESA/RAAE, Mr Laird

TELEPHONE NUMBER: DSN 523-6290

PROJECT ADVOCATE: HQ AFCESA/DF, CMSgt Reyff

TELEPHONE NUMBER: DSN 523-6156

#### **ABSTRACT**

This plan specifies procedures to evaluate a commercially developed aqueous film forming foam (AFFF) metering system installed in an A/S32P-19 firefighting vehicle. The system can be controlled by the vehicle operator without dismounting or relinquishing control of the vehicle. Headquarters Air Force Civil Engineering Support Agency, Firefighting and Facilities Branch, has overall responsibility for program management. The Responsible Test Organization, HQ AFCESA/RACF, will conduct the evaluation at Tyndall AFB, Florida, at Fire Research Facility #1. One off-the-shelf AFFF metering system manufactured by Nordic Systems Inc. will be evaluated. The primary focuses of this evaluation are to examine the metering accuracy, system performance, operational effectiveness, and suitability of the AFFF system. The results of the evaluation will be used to support a decision to modify existing firefighting apparatus.

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#### **ABBREVIATIONS**

AQUEOUS FILM FORMING FOAM AFFF

AFR AIR FORCE REGULATION

OPERATIONAL AVAILABILITY Αo

CRASH FIRE RESCUE CFR

DEPARTMENT OF DEFENSE DOD

DEFENSE SWITCHING NETWORK DSN

**GALLON** gal

GALLONS PER MINUTE gpm

HEADQUARTERS AIR FORCE CIVIL ENGINEERING SUPPORT HQ AFCESA

AGENCY

IN ACCORDANCE WITH IAW

LIMITED TECHNICAL INSPECTION LTI

MISSION CAPABLE MC MDT MEAN DOWN TIME

MEASURE OF EFFECTIVENESS MOE

MEAN TIME BETWEEN MAINTENANCE MTBM

NATIONAL FIRE PROTECTION ASSOCIATION NFPA

NOT MISSION CAPABLE NMC

A/S32P-19 CRASH FIRE RESCUE VEHICLE P-19

RELIABILITY, MAINTAINABILITY, AND AVAILABILITY RESPONSIBLE TEST ORGANIZATION RM&A

RTO

## SECTION I INTRODUCTION

- 1.1 <u>Purpose</u>. Headquarters Air Force Civil Engineering Support Agency (HQ AFCESA), Firefighting and Facilities Branch (RAAE), will manage a product evaluation to verify metering accuracy, operational effectiveness, and suitability of the Nordic Systems Inc. Mark IIA Computerized Foam Proportioning System (hereafter called Mark IIA). The evaluation will be conducted by the Responsible Test Organization (RTO), HQ AFCESA/RACF, from 13 July through 9 November 1992, at Fire Research Facility #1, Tyndall AFB, FL. HQ AFCESA/RAAE will use the data collected to compare the aqueous film forming foam (AFFF) metering accuracy, foam discharge pattern, and hydrocarbon fire extinguishing capability of the Mark IIA with two other systems: the orifice plate system currently employed on the P-19 and the Hypro Corporation's metering system previously evaluated by RACF. The results of the evaluation will support a decision to retrofit Air Force AFFF firefighting apparatus. If applicable, the Department of Defense (DOD) could use the results of the evaluation for other firefighting vehicles.
- 1.2 System Description. The Mark IIA AFFF metering system is a computerized foam proportioning system. Nordic Systems Inc. personnel will install and calibrate the Mark IIA system on RACF's P-19 firefighting vehicle used in the evaluation and provide operator and maintenance training to evaluation participants. The system is government property and will be available for other test purposes if required. During the Mark IIA installation, Nordic Systems Inc. personnel will require some assistance from RACF personnel to install sight gauges on the water and AFFF tanks, and provide information on the P-19 water The Mark IIA system consists of: a computer, foam flow meter, solutions flow meter, foam control valve, a self-contained digital read-out unit, and associated wiring and electrical connectors. The Mark IIA computer program has been modified to meet current USAF objectives to provide foam in concentrates of 1.0%, 3.0%, and 6.0% at flow rates between 60 and 500 gallons per minute (GPM). The AFFF dispensing ratio of the Mark IIA system is switch selectable over a range of 0-6.0% AFFF by the operator from the cab of the vehicle. After the AFFF reservoir is serviced with foam concentration, the vehicle operator can adjust the Mark IIA the match the AFFF concentration in the reservoir.

- 1.3 <u>Background</u>. The DOD currently uses AFFF concentrates formulated and mixed with water in ratios of 3 and 6 percent, using an around-the-pump proportioning system with fixed orifices. Common fire protection community terminology refers to an AFFF concentrate designed to be mixed with water at a ratio of 3% AFFF to 97% water as "3% AFFF". A "6% AFFF" concentrate contains approximately one-half of the surfactant and other active ingredients as 3% AFFF concentrate per unit volume and, consequently, is referred to as "less concentrated". When mixed with water at their designed ratios, both types AFFF/water mixture are essentially the same. By using 1.0% AFFF concentrate (as compared to 3% and 6%), agent conservation and extended firefighting capability should be realized. Six percent foam concentrate will be evaluated to provide system performance data in case situations arise again where the Air Force "borrows" 6.0% foam from the Navy during Desert Storm. This product evaluation will be accomplished as part of a continuing effort to identify an AFFF system capable of metering foam accurately at 1% concentration.
- 1.4 <u>Objectives</u>. The primary objectives of this evaluation are to verify the AFFF metering accuracy and consistency of the Mark IIA system in the P-19 firefighting vehicle. The secondary objectives are to determine the effects of the Mark IIA system on the foam discharge pattern and the ability to produce quality foam. This evaluation will assess the Mark IIA system performance, operational effectiveness, and suitability for use with the P-19. The specific objectives are:
- 1.4.1 Objective E-1. Assess the Mark IIA system/P-19 integration and vehicle modification procedures.
- 1.4.2 Objective E-2. Assess the operational performance of the Mark IIA system installed on the P-19.
- 1.4.3 Objective S-1. Assess the compatibility of the Mark IIA system installed on the P-19 with firefighting operations.
- 1.4.4 Objective S-2. Assess the adequacy of technical data provided with the Mark IIA system.
- 1.4.5 Objective S-3. Assess the Mark IIA system Reliability, Maintainability, and Availability (RM&A).

- 1.5 Evaluation Concept and Scope.
- 1.5.1 Prior to modifying the P-19 vehicle with the Mark IIA system, the RTO will demonstrate the AFFF metering accuracy, foam discharge pattern, and foam quality of the existing orifice plate system. The results will be documented, and a performance baseline created for comparison with the Mark IIA system. After the orifice plate system has been baselined, the Mark IIA system will be installed on the same P-19 vehicle and the same AFFF metering accuracy, foam discharge pattern, and foam quality data will be collected on the Mark IIA.
- 1.5.2 Evaluation Conditions. The evaluation participants from RACF/ARA will be task qualified firefighting and maintenance personnel. Fire suppression capability demonstrations will consist of a 300 gallon hydrocarbon fire set in the RACF Fire Research Facility #1 pit. At the conclusion of each foam percentage evaluation, the AFFF metering accuracies and foam discharge patterns will be measured using the sight gauges and spray measurements to evaluate the repeatability of the Mark IIA system to consistently provide 1.0%, 3.0%, and 6.0% AFFF.
- 1.5.3 Procedures. AFFF metering accuracy evaluation data requirements are outlined in the data forms 6, 7, and 8. Foam discharge pattern evaluation procedures and data requirements are outlined in NFPA Standard 412. General firefighting practices and procedures as outlined in Air Force Regulation (AFR) 92-1, Fire Protection Program, will be followed. The safety and protection of personnel and equipment will take priority over accomplishing any evaluation task or objective.
- 1.5.4 Authority for the Mark IIA system product evaluation is in PMD 8028(9), dated 10 May 1991. This evaluation will be conducted as directed in AFR 80-14 and AFR 55-43, and a final report will be released for publication no later than 45 calendar days after the final evaluation data are collected processed.
- 1.5.5 Mark IIA system reliability data will be reported as mature system point data since the system is commercially available (off-the-shelf).

### SECTION II OBJECTIVES AND EVALUATION METHODOLOGY

- 2.1 <u>General Method of Accomplishment</u>. The capabilities of the Mark IIA system installed on a P-19 fire truck will be assessed for AFFF metering accuracy, foam discharge pattern, and fire suppression of controlled aircraft type hydrocarbon fires set in RACF's Fire Research Facility #1. The data on system performance, operational effectiveness and suitability will be recorded and reported as point data due to the relatively short evaluation period. Incompatibilities between the system and operational requirements will be documented on data forms provided and will include the procedures followed leading to the noted incompatibility, suggested corrective procedures, suggested hardware changes, and actions required to continue with operations.
- 2.2 <u>Objective E-1</u>. Assess the Mark IIA system/P-19 integration and vehicle modification procedures.
- 2.2.1 Measure of Effectiveness (MOE) and Evaluation Criterion. The MOE is noninterference. The criterion is no mutual interference between or among the P-19 and the Mark IIA system.
- 2.2.2 Method. Nordic Systems technicians will be assisted by RACF personnel during the installation and calibration of the Mark IIA system in the P-19 evaluation vehicle. They will perform a limited technical inspection (LTI) and functionally operate the Mark IIA modification prior to beginning the evaluation. RACF/ARA/BDM personnel will compare the installed hardware and components to the technical data package provided by Nordic Systems Inc. to verify completeness. The orifice plate system removed from the P-19 will be inventoried, inspected for completeness and apparent serviceability, and stored by RACF.
- 2.2.3 Data Requirements.

Element
Inputs from Evaluation Manager
Inputs from Evaluation Participants

Source
Data Forms 1 and 3

- 2.2.4 Data Collection and Processing. Evaluation participants will collect, compile, and categorize data during the evaluation. The Evaluation Manager will have primary responsibility for ensuring the accuracy and validity of the data collected. Data forms will be completed as required. The evaluation data will be the basis of the evaluation report.
- 2.3 Objective E-2. Assess the operational performance of the Mark IIA system installed on the P-19.
- 2.3.1 MOE and Evaluation Criteria. The MOE is Mark IIA system performance. The criteria are that the Mark IIA system consistently repeat metering accuracy, foam discharge patterns, and fire suppression capabilities.
- 2.3.2 Method. The P-19 vehicle water and AFFF tanks will be calibrated following the Firefighting Vehicle Fluid Calibration Procedures in data form 5. The P-19 and Mark IIA systems will be serviced and prepared for use in accordance with applicable technical manuals. After preparation for use, the P-19 and Mark IIA systems will be operated to dispense AFFF ten times from each turret/nozzle (roof, bumper, and handline) for 60 seconds with 1%, 3%, and 6% AFFF. After each

60 second dispensing operation, the water and AFFF tank quantities will be recorded using fluid sight gauges on the vehicle to determine the amounts used. This will be accomplished to compute the Mark IIA system metering accuracy and to determine repeatability with the various AFFF concentrations. The handline is included to determine the Mark IIA's ability to accurately meter AFFF at the lower flow rate of 60 GPM. To determine AFFF dispersal pattern consistency, the procedures in NFPA Standard 412, paragraph 4-1, Turret Ground Pattern Test, will be followed. The Mark IIA system will then be employed IAW standard firefighting procedures to extinguish 300 gallon pit fires to demonstrate fire suppression capabilities with 1%, 3%, and 6% AFFF concentrations. During dispensing operations, special attention will be given to the Mark IIA system performance. Incompatibilities between the Mark IIA system and the P-19 fire truck or other CFR equipment will be recorded in detail. Likewise, enhanced capabilities due to the Mark IIA system performance or its interface with other CFR equipment will be recorded in detail.

During the live fire events, the Evaluation Manger will insure compliance with the safety procedures identified in Section IV.

2.3.3 Data Requirements.

Element
Inputs from Project Manager
Inputs from Evaluation Participants

Source
Data Forms 1 through 8

- 2.3.4 Data Collecting and Processing. Evaluation participants will collect, compile, and categorize data during the evaluation. The Evaluation Manager will have primary responsibility for ensuring the accuracy and validity of the data collected. Data forms will be completed as required. The evaluation data will be the basis of the evaluation report.
- 2.4 Objective S-1. Assess the compatibility of the Mark IIA system with the P-19 firefighting vehicle.
- 2.4.1 MOE and Evaluation Criterion. The MOE is compatibility among and between all components of the Mark IIA system and the P-19 in the operational environment. The criterion is that the performance of the Mark IIA system neither prevent nor hinder successful performance of any evaluation event.
- 2.4.2 Method. The Mark IIA system will be employed as described in paragraph 2.3.2 and maintained IAW the operational concept and the manufacturer's technical data. The evaluation participants will be briefed to be alert for any actual or foreseeable compatibility problems between and among the components. The evaluation participants will notify the Evaluation Manager of any observed or experienced compatibility problems. The Evaluation Manager will record their comments in the Evaluation Manager's Log.
- 2.4.3 Data Requirements.

Element
Inputs from Project Manager
Inputs from Participants

Source
Data Forms 1,2,3 and 4

2.4.4 Data Collection and Processing. Same as Paragraph 2.2.4.

- 2.5 <u>Objective S-2</u>. Assess the adequacy of the vendor provided technical manuals for the Mark IIA system.
- 2.5.1 MOE and Evaluation Criteria. The MOE is the adequacy of the technical manuals as judged by evaluation participants. The criteria are that the documents be written so a task-qualified technician can readily understand and follow the procedures and, by following the procedures, achieve the intended outcome.
- 2.5.2 Method. During this evaluation, participants will use the vendor provided technical manuals. After each evaluation event, the participants will indicate, on data forms and maintenance logs, any difficulties that prevented or hindered successful task performance. The Evaluation Manager will record reported problems, pertinent observations, and comments in the Evaluation Manager's Log.
- 2.5.3 Data Requirements.

<u>Element</u> Inputs from Project Manager Inputs from Participants Source
Data Forms 1,2,3 and 4
System Operator's Manual

- 2.5.4 Data Collection and Processing. At the conclusion of the evaluation, the team will compile the collected data. Technical manual deficiencies will be reviewed and verified prior to inclusion in the evaluation report. The Evaluation Manager will be responsible for ensuring reported technical manual deficiencies are clearly and completely explained.
- 2.6 Objective S-3. Assess the Mark IIA system Reliability, Maintainability, and Availability (RM&A).
- 2.6.1 MOE and Evaluation Criterion. The MOE is system RM&A. There is no criterion established for this system.
- 2.6.2 Method. The system will be employed as described in this section. The Evaluation Manager and participants will record system failure and repair data. These data will be used to calculate system point RM&A rates for the evaluation period.
- 2.6.3 Data Requirements. Same as paragraph 2.5.3.
- 2.6.4 Data Collection and Processing. The evaluation participants will collect, compile, and categorize data during the evaluation. The Evaluation Manager will have primary responsibility for ensuring the accuracy and validity of the data collected. Failures will be recorded and reported in chronological order on data forms. The failure data will be used to calculate the Mean Time Between Maintenance (MTBM), Mean Down Time (MDT), and Operational Availability (Ao) as follows:

MTBM = TOTAL OPERATING TIME

TOTAL NUMBER OF MAINTENANCE EVENTS

### MDT = TOTAL NUMBER OF REPAIR ACTIONS

Maintenance Events for MTBM calculations are defined as any maintenance action required to correct a Mark IIA system or component malfunction which renders it not mission capable. P-19 fire truck failures will be recorded but not charged to the Mark IIA system RM&A rates. The total operating hours shall be the sum of the hours taken from the Operational Status Log and will include the total time the system was in use. The time the system is not serviceable due to a failure will not be included as operating hours. The MDT will not include time lost due to the non-availability of replacement components. The system developed for this evaluation was not provisioned with spare/replacement components; therefore, the time required to arrange for the replacements from the vendor will not be charged against the system. Repair time will count only the time required to troubleshoot and physically repair the actual failure. The Ao will be expressed as the percentage of time the system is available for use with respect to the total time required for use.

#### SECTION III MANAGEMENT AND RESOURCES

#### 3.1 Management Relationships.

COULDMENT ITEMS

3.1.1 HQ AFCESA/RAAE will exercise overall program direction and provide funding for the Nordic Systems Inc. Mark IIA AFFF computerized metering system evaluation. HQ AFCESA/RACF, the Responsible Test Organization (RTO), will conduct the evaluation and provide the data collected to RAAE for analysis and reporting.

3.1.2 HQ AFCESA/RACF will organize evaluation events, collect and correlate data, and provide security, storage, and personnel support for the evaluation. Upon completion of the evaluation, RACF with RAAE will publish an evaluation report within 45 days of receipt of the compiled evaluation data.

3.2 <u>Key Personnel</u>. Table 1 lists personnel who are responsible for evaluation planning, implementing, and reporting.

	TABLE 1.	KEY PERSONNEL	
<u>Title</u>	Name/Grade	Organization	<u>Phone</u> (DSN)
Project Sponsor	Mr Laird	HQ AFCESA/RAAE	523-6290
Project Advocate	CMSqt Reyff	HQ AFCESA/DF	523-6156
Project Manager	Mr Ğrimm	HQ AFCESA/RAAE	523-6303
Evaluation Manager	Mr Vickers	HQ AFCESA/RACF	523-3734
Project Engineer	Mr Pike	HQ AFCESA/DFE	523-3742
Technical Ădvisor	Mr Wilson	ARA	523-3169
Technical Advisor	Mr Dees	ARA	523-3169

- 3.3 Resources. HQ AFCESA/RACF will provide facilities, consumables, equipment, and personnel to support this evaluation.
- 3.3.1 Evaluation Support. Table 2 lists evaluation support requirements.

#### TABLE 2. EVALUATION REQUIREMENTS

QUANTITY MODIFIED A/S32P-19/Mark IIA PORTABLE VIDEO CAMERA 35 MILLIMETER STILL CAMERA STOPWATCH 100-FOOT MEASURING TAPE	l (full time) l (during events l (during events 2 (during events l (during events
CONSUMABLE ITEMS QUANTITY FUEL (SUITABLE FOR LIVE FIRE EVENTS) 1/2-INCH VIDEO TAPE 35 MILLIMETER FILM (COLOR SLIDES and PRINTS) WATER AFFF 1% 3% 6%	800 gallons 5 each 5 rolls 18,000 gallons 250 gallons 600 gallons 1100 gallons
FACILITIES MAINTENANCE BAY STORAGE BAY FIRE PIT	l (as required) l (as required) l (as required)

3.3.2 The Evaluation Manager is authorized to contact Nordic Systems Inc. directly, as necessary, to aid in accomplishing this evaluation; however, he may not offer to purchase or obligate the Air Force in any way. This must be clearly stated in all communications with commercial vendors. As soon as it is practical, the Evaluation Manager will notify HQ AFCESA/DF and RAAE of any reportable evaluation related personnel injury or catastrophic system failure, caused by or relating to the use of the P-19/Mark IIA system. At the completion of the evaluation, the Evaluation Manager will collect and compile the data required to publish an evaluation report. HQ AFCESA/RAAE will prepare the evaluation report.

#### 3.4 Release of Information.

- 3.4.1 HQ AFCESA/PA, DSN 523-6476, is responsible for information coverage of this evaluation. Clearance of information will be in accordance with AFR 190-1, Public Affairs Policies and Procedures, Chapters 6 and 9. News releases, if any, will spotlight the evaluation purpose, equipment, methods, and participating personnel. No value judgement will be made.
- 3.4.2 The Evaluation Manager is responsible for informing HQ AFCESA/DF and RAAE of any incident or mishap. The releasing authority for information on any incident or mishap is HQ AFCESA/PA, through the safety office of the evaluation location or the base public affairs officer, after coordination with the HQ AFCESA/CC. Releases will be made in accordance with AFR 190-1.

#### SECTION IV SAFETY PLAN

4.1 <u>Purpose</u>. General firefighting practices and procedures are outlined in Air Force Regulation (AFR) 91-1, <u>Fire Protection Program</u>, will be followed throughout the evaluation. The safety and protection of personnel and equipment takes priority over accomplishing any evaluation objective. Every effort will be made to prevent deviating from preplanned actions, and standard operating practices and procedures. Deviations may only be authorized by the evaluation manager with the concurrence of the AFCESA safety officer. This Safety Plan establishes the safety areas for live fires using partial percentage AFFF. Live fires will be conducted at the AFCESA Fire Research Facility #1. This document contains detailed safety rules which govern the conduct of this evaluation series. The Evaluation Manager will act as Supervisor of Fire Test (SOFT) and will ensure adherence of all safety policies. Before conducting any live fires at the Fire Research Facility, the Base Fire Department Communications Center will be notified. The following documents are applicable to this test:

AFOSH 127-40 & 42, Emergency Eye Wash AFOSH 127-11 & 50, First Aid Kits AFOSH 127-31, Personal Protective Clothing and Equipment AFR 92-1, Paragraph 4-14, Safety Equipment for Fire Fighters AFR 127-4, Accident Reporting

4.2 <u>Overall Safety Responsibility</u>. HQ AFCESA/RACF, as Evaluation Manager, is responsible for enforcing the overall safety program for the evaluation. The Evaluation Manager or his designated representative will act as the Safety Officer during all fire events at the test site.

#### 4.3 <u>General Safety</u>.

- 4.3.1 <u>Safety Briefing</u>. The Evaluation Manager will inform all test personnel on known safety hazards associated with this test and test site. Supervisors will, in turn, inform their personnel on these hazards.
- 4.3.2. <u>Visitors</u>. Visitors will be permitted at the test site only with the approval of the Evaluation Manager. Visitors will be instructed on applicable safety regulations.
- 4.3.3. <u>Individual Safety Responsibility</u>. Careful attention to potential hazards associated with fire testing must be stressed at all levels of responsibility. The purpose of the safety rules outlined herein is to present the most important elements in experimenting with controlled fires. These rules do not cover all the possible hazards which may occur at the site. As new problems arise, new safety measures must be established. This Safety Plan must be strictly adhered to by all personnel and enforced by all supervisors.
- 4.3.4 <u>First Aid</u>. A first-aid kit will be maintained at the site and all personnel will be informed on its location.
- 4.4 Accident Reporting (Emergency).
- 4.4.1 <u>Scope</u>. The purpose of this procedure is to ensure expedient handling and care of personnel injured in an accident or disaster. All post-emergency reporting and investigation of an accident will be performed in accordance with applicable Air Force regulations.

- 4.4.2 <u>Responsibility</u>. Each person involved in this program must be familiar with the emergency reporting procedures established by this plan and immediately implement these procedures in the event of an accident. The Evaluation Manager will ensure that all supervisors and subordinates are familiar with this procedure.
- 4.4.3 <u>Emergency Reporting Procedures</u>. In the event of an accident at the test site, the following procedures will be followed:

a. The Evaluation Manager will direct appropriate first aid. Caution will

be exercised to prevent aggravation of an accident-related injury.

b. Tyndall Air Force Base Hospital Ambulance Service will be notified by calling extension 911. The nature of the accident, including apparent condition of injured personnel and the location of the test site, will be reported to the medical personnel. The Evaluation Manager or his designated representative will decide whether to transfer the injured directly to a hospital or to request emergency ambulance support.

c. The Evaluation Manager or his designated representative will determine the seriousness of the accident. If the accident is not serious enough to require emergency hospitalization or ambulance service, the injured person will

be taken to a doctor or hospital by normal means of transportation.

d. All accidents requiring emergency treatment or first aid must be reported to the AFCESA Safety Officer.

- 4.5 Fire Prevention, Reporting, and Emergency Procedures.
- 4.5.1 <u>Responsibility</u>. The Evaluation Manager will be responsible for the implementation of the procedures established by this plan. All on-site personnel must be completely familiar with these procedures to ensure proper response to an emergency.
- 4.5.2 <u>Fire Prevention Procedures</u>. The procedures listed in Check List #1 are to be followed in an effort to reduce chances of an uncontrolled fire.
- 4.6 <u>Test Site Location</u>. All fire evaluations will be conducted at the 100 foot AFCESA Fire Research Facility #1, located on Farm Dale Road. These tests will be conducted in accordance with AFCESA Office Instruction dated 7 April 1988, entitled "Live Fire Demonstration/Tests". The following checklist will be used prior to conducting live fire evaluations.

# CHECK LIST #1 TO BE USED BEFORE CONDUCTING LIVE FIRES AT FIRE RESEARCH FACILITIES NO. 1

DATE:	
<u>VERIFIED</u> <u>PROCEDURES</u>	
Inform all personnel on proper safety precautions. All personnel at the test site are needed to support the test or approved visitor?	· an
Inform all personnel on accident and fire reporting procedures Radio or telephone communications available? Inform all personnel of the telephone numbers for the ambulance and	fire
department Ensure a first aid kit is available Ensure an emergency eye wash station is available.	
Ensure all fuel valves are closed and there are no fuel	
leaks prior to fuel ignition Secure area prior to igniting fire.	
4.7 Notification. Before conducting a fire test, notify the Fire Department Communications Center at Extension 3-2884. The Fire Department Communicat Center will need an estimate of the duration of the live fire tests.  Communications Center will be requested to notify the following:  a. Command Post - 3-2155  b. Air Traffic Control Tower - 3-4553  c. Base Hospital - 3-7514  d. Security Police - 3-2028  e. Division of Forestry - 3-2641  f. Base Weather - 3-2856	ions

#### ANNEX 1

DATA FORMS

AN ABBREVIATED SET OF DATA FORMS ARE INCLUDED ON THE FOLLOWING PAGES

# DATA FORM #1 EVALUATION MANAGER'S LOG

DAT	E	EVENT & COMMENT
		DATA FORM # 2 FAILURE LOG
DATE	FAILURE (	CLASSIFICATION / CAUSE / CORRECTIVE ACTION
		DATA FORM # 3 EVALUATION EVENT LOG
DATE	EVENT	COMMENT
DDITIC	NAL COMMENTS:	

### DATA FORM # 4 OPERATIONAL STATUS LOG

DATE	TIME	STATUS	COMMENT
-			
		<u> </u>	

STATUS CODES:

MC - MISSION CAPABLE, THE SYSTEM IS READY FOR USE.

NMC - NOT MISSION CAPABLE, THE SYSTEM CANNOT BE USED DUE TO A HARD FAILURE.

NMR - NOT MISSION READY, THE SYSTEM IS OUT OF SERVICE FOR A SCHEDULED INSPECTION OR SERVICING (NOT A SYSTEM FAILURE). "NMR TIME" WILL BE COUNTED AS "MC TIME" FOR PURPOSES OF CALCULATING SYSTEM RM&A DATA UNLESS A FAILURE IS DISCOVERED DURING THE MAINTENANCE ACTION.

### DATA FORM # 5 FIRE FIGHTING VEHICLE FLUID CALIBRATION PROCEDURES

- A. Water Tank Calibration.
- 1. Ensure that water tank is empty.
- Ensure that the vehicle is parked on a level surface throughout tank calibration procedures.
- Using a liquid flow meter, fill tank in 50 gallon increments, to its 1,000 gallon capacity, and calibrate a tank level indicator (dip stick) at 50 gallon increments.

DATA SHEET WATER TANK

- B. AFFF Tank Calibration.
- 1. Ensure that AFFF tank is empty.
- Ensure that the vehicle is parked on a level surface throughout tank calibration procedures.
- Using a liquid flow meter, fill AFFF tank in 5 gallon increments, to its 130 gallon capacity, and calibrate a tank level indicator (dip stick) at 5 gallon increments.

DATA SHEET AFFF TANK

	Vehicle Ructors:	egistration Number:	Date: Evaluator:		Registration Number:
F	ill Water oint <u>Gallons</u>	Water	Fill <u>Point</u>	AFFF <u>Gallons</u>	AFFF Depth
	1		1 2		<del></del>
	3		3		
	5 6 ————		5 6		
	8		, 8 9		
1 1	0		10 11		
1	3		12 13		-
1 1 1	5	<u> </u>	14 15 16		
1	7		17 18		
1:			19 20		

### ALL METERING SHEETS IN ORIGINAL TEST PLAN INCLUDED 10 RUNS UNDER EACH CATEGORY

# DATA FORM # 6 1% AFFF METERING TEST MATRIX AND DATA COLLECTION SHEET

TEST NO. <u>TURRET</u>		G WATER TANK ) START END	AFFF TANK WAT START END USE	AMB. TEST TEMP DATE
1-10 ROOF	1% AFFF 60			 
1-10 BUMPER	1% AFFF 60			 
1-10 RF/8MP	1% AFFF 60			 
1-10 HNDLNE	1% AFFF 60			 

# DATA FORM # 7 3% AFFF METERING TEST MATRIX AND DATA COLLECTION SHEET

	AFFF DISPENS TANK TIME (s	ING <u>WATER TANK</u> ec) <u>START END</u>	AFFF TANK START END	WATER USED	AFFF USED	RATIO	AMB. TEMP	TEST DATE
1-10 ROOF 3	% AFFF 60	-						
1-10 BUMPER 3	% AFFF 60							
1-10 RF/BMP 35	% AFFF 60							<del></del>
1-10 HNDLNE 33	% AFFF 60							

# DATA FORM # 8 6% AFFF METERING TEST MATRIX AND DATA COLLECTION SHEET

TEST NO. <u>TURRET</u>	AFFF DISPENSING TANK TIME (sec)		AFFF TANK START END	WATER USED	AFFF USED	RATIO	AMB. TEMP	TEST <u>DATE</u>
1-10 ROOF	6% AFFF 60	<del></del>						
1-10 BUMPER	6% AFFF 60	<del></del>						
1-10 RF/BMP	6% AFFF 60							
1-10 HNDLNE	6% AFFF 60	<del></del>						

NOTE: RF/BMP = ROOF and BUMPER

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